

# сообщения ОбъЕДИНЕННОГ ИНСТИТУТа ядерных исследований 

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## SYNCHROTRON RADIATION CALCULATIONS

 AND COLLIMATOR DESIGNFOR THE TAU-CHARM FACTORY

## I. INTRODUCTION

Design study of the high luminosity symmetric $e^{+}-e^{-}$ collider in Dubna (Tau-Charm factory) was published in /1,2/. The main accelerator parameters are: energy 2.2 GeV , total current $J=0.6 \mathrm{~A}$, horizontal emittance $\varepsilon_{\mathrm{x}}=4.110^{-7} \mathrm{~m}$, vertical emittance $\varepsilon_{y}=210^{-8} \mathrm{~m}$.

An important constraint on the design is the background expected from synchrotron radiation (SR) /3-6/. A care must to be taken in minimizing the $S R$ via the layout of the magnet system.


Fig. 1 Layout of the magnetic elements in the interaction region (IR) of the Tau-Charm factory. Several positions of the SYNRAD projection plane are shown: PP-A, PP-B, PP-C.

SR is produced when an electron or positron is bent in the magnetic field of a dipole or quadrupole. The magnetic lattice in the IR is shown on Fig. 1 - the $e^{+}$and $e^{-}$beams are separated symmetrically by the use of the electrostatic separator $E S$, the offset quadrupole $Q 4$ and the bending magnets BV1 and BV2. Minimal beam dimensions at the
interaction point (IP) are achieved by means of the low $\beta$ S.C. quadrupoles $\mathrm{Q} 1, \mathrm{Q} 2, \mathrm{Q} 3$.

The thin beampipe (Fig.1) made from beryllium and lined with a thin layer of Cu is centered around the IP and separates the detector and accelerator volumes. To protect the beampipe from direct $S R$ some masks must be foreseen on either side of the IP. Most of the SR photons pass trough the IR without interaction or are adsorbed in the masks and in the chamber walls. Due to Compton scattering and induce fluorescence some secondary photons appear, which may pass trough the beam pipe and enter the detector.

The acceptable level of backgrounds are is defined by the following criteria $/ 3,4,6 /$ : the maximal dose which the detector can stand without being damaged, the maximal occupancy, i.e: the highest tolerable probability of background hits and the maximum heat load for which adequate cooling of the beampipe can be supplied. Because of its proximity to the IP, silicon vertex detector is most subject to radiation damage. For a minimum lifetime of $10^{7}$ s the energy deposition per time and area in $200 \mu \mathrm{~m}$ thick silicon layer must not exceed $10^{-9} \mathrm{~W} / \mathrm{cm}^{2}$. For the central track chambers an occupancy of several percent is considered the limit of for proper performance.

## II. SR SIMULATION PROGRAM

We present a fast algorithm for determination the $S R$ intensity incident on the surfaces of interest (e.g. the vacuum chamber walls, the beampipe, the mask sides, the ES electrodes). The program SYNRAD works in interactive regime displaying the topology of the $S R$ spots on these surfaces. The maximum calculation time needed (for integration over the total photon energy interval) is less than 10 min . SYNRAD uses many of the ideas already suggested in similar SR-modeling programs /3,4/.

SYNRAD works in the following way. First, an
appropriate plane is defined by the user - we refer to it bellow as projection plane (PP). No restrictions on the slope of $P P$ or on its distance to the IP are assumed, but it must be perpendicular to the $Y Z$-plane and must cross the SR fan (or fans). Secondly, the $S R$ produced by the beam passing trough one or several magnetic elements is projected on the projection plane and the distribution of power density (or number of photons/s) is compiled. Choosing the PP position so that it coincides or is tangential to the surfaces of interests we obtain picture of the $S R$ propagation in the interaction region.

We choose rectangular coordinate systems:

1) beam coordinate system ( $\vec{z}, \overrightarrow{x, y})$ with origin in the current point s, the $\vec{y}$-axes lies in the central trajectory plane, the $\vec{Z}$-axes is tangential to the central trajectory.
2) laboratory coordinate system ( $\vec{X}, \vec{Y}, \vec{Z}$ ) with origin in the IP, the $\vec{Y}$-axes lies in the central trajectory plane.
3) transversal coordinates on the PP: ( $\left.x_{w}, y_{w}\right)$.

The program accepts as input:

- a machine lattice file produced by MAD, in which magnet positions, lengths and strengths are specified;
- the central beam trajectory $Y_{c}(s), Z_{c}(s)$ and the beta functions as calculated by MAD; $s$ is the coordinate along the central beam trajectory;
- the beam energy ( 2.2 GeV ) and the horizontal and vertical emittances;
- the projection plane position in space;
- the photon energy interval required.

At the program output we obtain distribution of the $S R$ power density (or number of photons/s) on the projection plane. Some positions of the projection plane (PP-A, PP-B, $\mathrm{PP}-\mathrm{C}$ ) used in calculations are shown on Fig.1.

SYNRAD starts with calculating the central trajectory and the beam+stay-clear envelopes $\sigma_{x}(s)$ and $\sigma_{y}(s)$ with step 1 cm over the longitudinal coordinate $s$ inside every
magnetic element ( SPLINE method). A simplifying assumption in the beam model consist in neglecting the width of the phase space ellipse, thus assuming definite correlation between $x$ and $x^{\prime}=d x / d s$ and between $y$ and $y^{\prime}=d y / d s / 3 /$. This makes it possible to define a 3D velocity field $\vec{v}(s, x, y)$. At each beam point $s, x, y$ the direction of $\overrightarrow{\boldsymbol{V}}$ is defined by

$$
\begin{equation*}
\operatorname{tg}\left(\alpha_{\mathrm{x}}\right)=\left(\sigma_{\mathrm{x}}^{\prime} / \sigma_{\mathrm{x}}\right) \mathrm{x} ; \quad \operatorname{tg}\left(\alpha_{\mathrm{y}}\right)=\left(\sigma_{\mathrm{y}}^{\prime} / \sigma_{\mathrm{y}}\right) y \tag{1}
\end{equation*}
$$

where $\alpha_{x}, \alpha_{y}$ are angles between $z$-axes and the projections of the vector $\vec{v}$ on the $(\vec{x}, \vec{z})$ и ( $\vec{Y}, \vec{z}$ ) planes. The radiation of a pointlike $S R$ source located at $X_{s}, Y_{s}, Z_{s}$ is propagating along the line

$$
\begin{aligned}
& Y=\left(Z-Z_{s}\right) \operatorname{tg}\left(\alpha_{c}+\alpha_{y}+\varepsilon\right)+Y_{s^{\prime}} \\
& X=\left(Z-Z_{s}\right) \operatorname{tg}\left(\alpha_{x}\right)+X_{s}, \\
& \varepsilon= \pm 1 /(2 \gamma) ;
\end{aligned}
$$

$\alpha_{c}$ is the angular offset (for fixed $s$ ) of the central trajectory: $\quad t g\left(\alpha_{c}\right) \equiv d Y_{c} / d Z_{c}$. The parameter $\varepsilon$ appears because of the angular spread of the $S R$ in the $\vec{Y}, \vec{Z}$ plane (see below).

Point to point transformation
Let ( $x_{w}, Y_{w}$ ) are rectangular coordinates on the PP. For given $s$ the coordinates $x_{w}, y_{w}$ at which the line (2) intersects the $P P$ can be expressed by the source coordinates $x, y$ in terms of elementary functions, thus defining the transformation $(x, y) \rightarrow\left(x_{w}, y_{w}\right)$. However, the reverse transformation $\left(x_{w}, y_{w}\right) \rightarrow(x, y)$ can be analytically found only in case that $\varepsilon=0$.

## Mapping

We first divide the $P P$ into rectangular cells $d x_{w 1} d y_{w j}$.
We divide the beam along its central trajectory into 1 cm segments and each segment in both transverse dimensions $x, y$ into current elements each having volume dxdyds. The
elementary radiation fan (Fig.2) is formed by four lines of the kind (Eq. 2 ) - the upper two with $\varepsilon=-1 /(2 \gamma)$ and the lower two - with $\varepsilon=1 /(2 \gamma)$. In such a way the $1 / \gamma$ angular spread of the radiation is taken into account only in vertical direction. The cross-section of the elementary fan with the $P P$ is an appropriate quadrangle (Fig.2). We assume that the $S R$ intensity radiated by the volume dxdyds is uniformly distributed over the quadrangle area, so this intensity should be distributed proportionally over the PPcells $d x_{w i} d y_{w j}$ (each cell is given a portion proportional to its fraction of quadrangle's area). Finally we integrate 1) over the transverse beam coordinates $x, y$ from $-10 \sigma$ to $10 \sigma$ multiplying at each point $x, y$ by the appropriate gaussian weight; 2) over the coordinate $s$ from the beginning to the end of the magnet; 3) over the photon energy interval (only in case of quadrupole).
 with taking into account the vertical $1 / \gamma$ angle spread of the SR.

SYNRAD divides the machine magnetic elements into two groups and uses different procedures of mapping for each group:

1) "near" sources (to the IP) - quadrupoles $Q 1, Q 2, Q 3$; the $1 / \gamma$ angle spread of SR is neglected so $\varepsilon=0$ and the reverse transformation $\left(x_{w}, Y_{w}\right) \rightarrow(x, y)$ is used. This sufficiently simplifies the calculations.
2) "distant" sources or bending magnets - ES, the offset quadrupole $Q 4$, BV1 and BV2. The $1 / \gamma$ angle spread of $S R$ is taken into account.

When calculating the $S R$ produced in the beam volume dxdyds we need to know the local radius of the electron trajectory. Inside the bending magnet ( $\mathrm{ES}, \mathrm{Q4}, \mathrm{BV}, \mathrm{BV} 2$ ) it is assumed to be constant ( $\rho=$ const) for all $x, y$. Inside $a$ quadrupole with strength $k$ :

$$
\rho(\dot{x}, y)=k^{-1}\left(x^{2}+y^{2}\right)^{-1 / 2}
$$

To verify the SYNRAD results we use the following criteria:

1. The total intensity radiated by any magnetic element must not depend on the steps $d x, d y, d z, d x_{w}, d y_{w}$, or on the $P P$ position in space. SYNRAD satisfies this with an accuracy better than $10^{-2}$.
2. The total power radiated by the beam passing a quadrupole must not be far from

$$
\begin{equation*}
P_{\mathrm{tot}}[\mathrm{~W}]=7 \cdot 10^{-8} \gamma^{4} J[\mathrm{~A}] \mathrm{K}^{2}\left(\bar{\sigma}_{\mathrm{x}}^{2}+\bar{\sigma}_{\mathrm{y}}^{2}\right) 1_{\mathrm{elem}} \tag{3}
\end{equation*}
$$

where $\quad \bar{\sigma}_{x, y}=\frac{1}{2}\left(\sigma_{x, y}^{\max }+\sigma_{x, y}^{\text {min }}\right)$,

$$
\sigma_{x, y}^{\max }=\max _{s}\left(\sigma_{x, y}(s)\right) ; \sigma_{x, y}^{\min }=\min _{s}\left(\sigma_{x, y}(s)\right),
$$

$I_{\text {elem }}=s_{\text {fin }}-s_{\text {beg }}$ is the quadrupole length in cm.
3. The total power and number of photons/s radiated by the beam passing a bending magnet can be found exactly:

$$
\begin{aligned}
& P_{\mathrm{tot}}[\mathrm{~W}]=8,57 \cdot 10^{-8} \gamma^{4} J[\mathrm{~A}] \rho^{-2}[\mathrm{~cm}] 1_{\text {elem }} ; \\
& \frac{d N}{d t} \text { tot }\left[\mathrm{c}^{-1}\right]=6,2 \cdot 10^{16} \gamma J[\mathrm{~A}] \frac{1 \mathrm{elem}}{\rho[\mathrm{~cm}]}
\end{aligned}
$$

## "Distant" sources

The parameters of the "distant" sources are shown in Table 1. The total number of photons/s and the total power in Table 1 are calculated by Eq. 4 . SYNRAD obtains the same values with an accuracy $10^{-3}$. This result does not depend on the position of PP .

Table 1. Parameters of the "distant" sources.

| bend | length <br> cm | $u_{c}$ <br> m | $d N /\left.d t\right\|_{\mathrm{tot}}$ <br> eV | $P_{\mathrm{tot}}$ <br> S |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| ES | 340 | $10^{3}$ | 23,6 | $5,410^{17}$ | 0,68 |
| Q4 | 60 | 112,3 | 210 | $8,510^{17}$ | 9,4 |
| BV1 | 50 | 59,5 | 397 | $1,310^{18}$ | 28 |
| BV2 | 70 | 41,6 | 567 | $2,710^{18}$ | 80 |

## Near" sources

The quadrupole parameters are given in Table 2. Here the total number of photons/sec, the total power and the average critical energy $u_{c}$ of the radiation are found by SYNRAD ( $u_{c}$ is defined as $u_{c} \approx 3 u_{\max }$, where $u_{\max }$ corresponds to the maximum of the spectrum. The corresponding values of $P_{\text {tot }}$ calculated by Eqn. 3 are shown in Table 3 .

Table 2. Parameters of the "near" sources.

| quadr. | length <br> cm | $k$ <br> $\mathrm{~m}^{-2}$ | $u_{\mathrm{c}}$ <br> eV | $d N /\left.d t\right\|_{\mathrm{tot}}$ <br> $\mathrm{s}^{-1}$ | $P_{\mathrm{tot}}$ <br> W |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Q1 | 50 | -3.66 | 150 | $3.810^{17}$ | 6 |
| Q2 | 50 | 3.55 | 300 | $410^{17}$ | 16 |
| Q3 | 20 | -3.51 | 180 | $1.110^{17}$ | 3 |

Table 3.

| quadrupole | $P_{\mathrm{tot}}, \mathrm{W}$ | Eqn.3 |
| :---: | :---: | :---: |
| Q1 | 6 | 4.8 |
| Q2 | 16 | 17.6 |
| Q3 | 3 | 3.8 |

SR in the interaction region
Here we discuss the power and photons/sec levels on all surfaces within $\pm 12 \mathrm{~m}$. We use the following positions of the Projection Plane (Fig.1): $P P-A: P P$ is tangential to the vacuum chamber wall (radius 6 cm );
PP-B: PP is normal to the beams and passes the IP;
PP-C: PP coincides with the lower pair of separator electrodes (at radius 5 cm ).

Power density along the vacuum chamber wall (radius $6 \mathrm{~cm}, \mathrm{PP}-\mathrm{A})$ ) is shown on Fig. 3 a . Fig. 3 b shows the topology of the corresponding $S R$ spot, its maximal transverse size is roughly 1 cm .

Fig. 4 shows the distribution near the $I P$ ( $P P-B$ ) of photons having energies more than 1 keV and produced inside the three quadrupoles $Q 1, Q 2, Q 3$. This radiation passes trough the detector region without striking any surfaces.

The electrostatic separator ES consists of two pairs of electrodes - upper and lower. Almost all the SR produced inside the magnet $B V 1$ passes trough the gap between the


Fig. 3a Power density, deposited by one bean into the vacuum chamber wall (radius 6 cm ):
a) linear power distribution;
б) a half of the $S R$ spot.


Fig. 4 SR intensity incident on the PP-B in units number phot. $>1 \mathrm{keV} / \mathrm{s} / \mathrm{mm}^{2}$, produced by the set of low $\beta$ quadrupoles $\mathrm{Q} 1, \mathrm{Q} 2, \mathrm{Q} 3$.
lower pair of electrodes. In the considered variant of magnetic system the magnet BV is divided into two parts (a weaker magnet BV1 and a stronger - BV2) in order to diminish $S R$ striking the separator. The $S R$ produced in the stronger magnet $B V 2$ does not reach the separator. Using position PP-C of the projection plane we find that if the gap size is 2 cm then the power density incident on the ES electrode is less than $5.10^{-3} \mathrm{~W} / \mathrm{cm}^{2}$.

## SR backgrounds without masks

We take the following parameters for the thin portion of the beampipe: radius 3.5 cm , length 24 cm , materials $25 \mu \mathrm{~m}$ $\mathrm{Cu}+1 \mathrm{~mm} \mathrm{Be}$.

Without masks $0.4 \mathrm{~W} /$ beam are incident on the beampipe surface corresponding to $3.210^{16}$ phot./s/beam. This SR is produced in the quadrupole Q4. The SR fans from the other magnets pass trough the $I P$ without striking any surfaces
(Q1,Q2,Q3); pass trough the narrow gap between the lower pair of ES-electrodes (BVI) or intercept the vacuum chamber wall near the separator (BV2).

The energy spectrum is quite soft as it can be seen in Table 4 (one beam).

Table 4. Energy spectrum of the photons striking the nonmasked beampipe

| phot. energy <br> interval | numb.phot./s |
| :---: | :---: |
| all (>0kev) | $3.210^{16}$ |
| $>1 \mathrm{keV}$ | $3.510^{13}$ |
| $>2 \mathrm{keV}$ | $8.510^{10}$ |
| $>4 \mathrm{kev}$ | $4.310^{6}$ |
| $>6 \mathrm{kev}$ | 300 |

The average power density incident on the beampipe surface is $7.7 \quad 10^{-4} \mathrm{~W} / \mathrm{cm}^{2} \quad\left(6 \quad 10^{13}\right.$ phot. $/ \mathrm{s} / \mathrm{cm}^{2}$ ). Taking $710^{-7}$ for the transmission coefficient we obtain that $5.4 \quad 10^{-10} \mathrm{~W} / \mathrm{cm}^{2}$ penetrate trough the beampipe and are incident on the first layer of silicon. This nears the allowed limit ( $10^{-9}$ ) so masking is necessary.

## Masking

Here we consider two variants of masking to shield the beampipe against direct radiation. The geometries are shown on Fig. 5 and Fig. 6 and the corresponding statistics of photons with taking into account reflection of photons from the mask tips and from the mask surfaces are shown on Tables 5 and 6. The average angle between the direction of the 04 -radiation fan and the $Z$-axes is 7 mrad .

In Variant 1 (short symmetric masks) two equal tantalum masks are situated symmetrically on the both sides of IP. The side 1 A of mask 1 doesn't have line-of-site to the detector beampipe so the reflected photons can not directly reach the detector. To estimate the number of photons scattered from the tip of mask 1 (Table 1) we use


Fig. 5 Variant 1 of masking (short symmetric masks). The angle between the $2 B$ side of mask 2 and the $Y$-axis is $87.5^{\circ}$. Number of photons scattered from the mask-1 tip $=210^{7}$. Of them $\sim 20$ phot./s enter the detector. Main background source ( $10^{6}$ phot./s) are the photons reflected from the side B2 (1.4 $10^{12}$ phot./s).
the method proposed in $/ 3 /$ - we assume that the corner of the mask has a $1 \mu \mathrm{~m}$ radius. The largest background source is backscattering of radiation from the side $2 B$. On this side Q4 deposits 1.3 W or $1.1 \quad 10^{17}$ phot./s distributed along 12 cm length down from the mask tip. Multiplying to an averaged solid angle fraction (0.016) and to the reflecting coefficient for Ta ( $810^{-4}$ ) we obtain that $1.410^{12}$ phot./s reflecting from the side $2 B$ strike the beampipe surface. Of these $10^{\circ}$ phot./s ( $1.210^{3}$ phot. $>1 \mathrm{keV} / \mathrm{s}$ ) penetrate the beampipe and enter the detector. In order to decrease this source of backgrounds we increase the slope of 2 B side which leads to asymmetric masks. These are considered in Variant 2.

|  | incidend on the mask numb.phot/s $s^{-1}$ | incident on the Be pipe numb. phot/s $s^{-1}$ | enter the detector numb.phot/s $s^{-1}$ |
| :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { mask } 1 \\ & >0 \mathrm{keV} \\ & >1 \mathrm{keV} \end{aligned}$ | $\begin{array}{ll} 6.5 & 10^{17} \\ 7.1 & 10^{14} \end{array}$ | $\begin{aligned} & 2.10^{7} \\ & 2.110^{4} \end{aligned}$ | $\begin{aligned} & 20 \\ & 0 \end{aligned}$ |
| $\begin{aligned} & \text { mask } 2 \\ & >0 \mathrm{keV} \\ & >1 \mathrm{keV} \end{aligned}$ | $\begin{aligned} & 1 \quad 10^{17} \\ & 1.3 \quad 10^{14} \end{aligned}$ | $\begin{array}{ll} 1.4 & 10^{12} \\ 1.7 & 10^{9} \end{array}$ | $\begin{gathered} 10^{6} \\ 1.210^{3} \end{gathered}$ |
| total <br> >0keV <br> >1 keV | $\begin{aligned} & \begin{array}{l} 7.5 \\ 10^{17} \\ 8.4 \end{array} 10^{14} \end{aligned}$ | $\begin{aligned} & 1.410^{12} \\ & 1.710^{9} \end{aligned}$ | $\begin{gathered} 10^{6} \\ 1.210^{3} \end{gathered}$ |

Table 5. SR backgrounds (from 1 beam) for Variant 1.


Fig. 6 Variant 2 of masking (long asymmetric masks). The angle between the 2 B side of mask 2 and the $Y$-axis is $88.5^{\circ}$. Photons reflected from side 1 A (1.4 $10^{11}$ phot./s) and from the side 2 B ( $610^{11}$ phot./s) are incident on the Be surface. Of them $5.210^{5}$ phot./s enter the detector.

In Variant 2 (long asymmetric masks) the length of the masks is increased. Although photons that scatter from side 1A have direct line-of-site to the detector beampipe the final backgrounds are even less than in Variant l. This is because the backscattering from side 2 B here is much lower.

|  | incident on the mask numb.phot/s $s^{-1}$ | incident on the Be pipe numb. phot/s $s^{-1}$ | enter the detector numb.phot/s $s^{-1}$ |
| :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { mask } 1 \\ & >0 \mathrm{keV} \end{aligned}$ | $6.510^{17}$ | $1.410^{11}$ | $10^{5}$ |
| >1 keV | $\begin{array}{ll}7.1 & 10^{14}\end{array}$ | $1.610^{8}$ | 110 |
| > 2 keV | $\begin{array}{lll}3.8 & 10^{12}\end{array}$ | $810^{5}$ | 0 |
| $\begin{aligned} & \text { mask } 2 \\ & \text { >okeV } \end{aligned}$ | $1.10{ }^{17}$ | $610^{11}$ | $4.210^{5}$ |
| >1 keV | $1.310^{14}$ | $7.610^{8}$ | 530 |
| >2keV | $8.210^{11}$ | $410^{6}$ | 3 |
| total |  |  |  |
| >0keV | 7.51017 | $7.410^{11}$ | $5.210^{5}$ |
| >1 keV | $8.410^{17}$ | $9.210^{8}$ | $640$ |
| > 2 keV | $4.610^{12}$ | $4.810^{6}$ | 3 |

Table 6. SR backgrounds (from 1 beam) for Variant 2.
Conclusions
SR Backgrounds in the C-Tau interaction region in absence of masks:

1) The maximal area density of SR power on the vacuum chamber wall is $1.4 \mathrm{BT} / \mathrm{CM}^{2}$ (from the magnet BV 2 ).
2) The maximal area density of $S R$ power incident on the edge of the ES lower electrodes is $510^{-3} \mathrm{BT} / \mathrm{CM}^{2}$ if the gap with between them is equal to 1 cm .
3) When passing the quadrupoles $Q 4$ the beams deposit
0.8 BT or $6.410^{16}$ phot./s (both beams) on the beampipe surface. The energy spectrum of this radiation is much softer than this obtained in design of B-factory /4/ there are practically no photons with energies of the $K$ lines of Cu ( 8 KeV ) causing induce fluorescence in the beampipe $C u$ coating. However masking of the direct $S R$ is necessary because of the high dose deposited on the first Si layer.

The both 1 -st and 2 -nd variants of masking diminish the power incident on the beampipe to $\sim 10^{-5} \mathrm{~W}$ and the photons to $\sim 210^{12}$ phot. $/ \mathrm{s}$. The total number of photons $/ \mathrm{s}$ entering the detector volume is $\approx 10^{6}$ phot./s, of them 1.3 $10^{3}$ have energy >1 kev and $\sim 10$ have energy $>2 \mathrm{keV}$.

According to the results obtained in $/ 3 /, / 4 /$ the occupancy of the central tracing chambers and the vertex detectors in such levels of backgrounds is negligible.

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