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# LORENTZ FRAMES' PARALLELISM AND THOMAS–WIGNER ROTATION

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#### Широков М.И. Параллельность лоренцевских систем и вращение Томаса-Вигнера

Предложено и обсуждено операционное определение параллельности двух лоренцевских систем отсчета. Оно позболяет уточнить понятия буста и общего преобразования Лоренца. Показано, что эта параллельность не обладает свойством транзитивности: если триада  $T_1$  осей системы  $S_1$  параллельна триаде  $T_2$  системы  $S_2$  и  $T_2 \parallel T_3$ , то, вообще говоря,  $T_1$  не параллельна  $T_3$ . Указанная нетранзитивность прямо связана с известным вращением Томаса–Вигнера. Ее учет необходим при обсуждении двух рассмотренных физических приложений вращения Томаса–Вигнера: прецессии Томаса и релятивистского фазового анализа.

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Shirokov M.I. Lorentz Frames' Parallelism and Thomas–Wigner Rotation

Operational definitions of the parallelism of two Lorentz frames are proposed and discussed. They allow to refine upon the notion of boosts and general Lorentz transformations. It is shown that the parallelism lacks the property of transitivity: if the triad  $T_1$  of a frame  $S_1$  axes is parallel to the triad  $T_2$  of  $S_2$  and  $T_2 \parallel T_3$ , then generally  $T_1$  is not parallel to  $T_3$ . This nontransitivity is directly related to the Thomas-Wigner rotation and clarifies the discussion of two considered physical applications of the rotation: Thomas precession and relativistic phase analysis.

The investigation has been performed at the Bogoliubov Laboratory of Theoretical Physics, JINR.

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## 1 INTRODUCTION

Before deriving the law of transformation between time-space coordinates of an event measured in two inertial frames  $S_1$  and  $S_2$ , one must at first specify the frames themselves. In the case of the special (pure) Lorents transformation (boost), the triple  $T_2$  of mutually orthogonal space axes of the reference frame  $S_2$  (named triad  $T_2$  below) is set to be parallel to the  $S_1$  triad  $T_1$ . However,  $T_2$  moves relative to  $T_1$ , and determination of their parallelism is more complicated as compared to the case when  $T_1$  is at rest relative to  $T_2$ . In the latter case, it is sufficient to measure the projections of each axis of  $T_2$  relative to  $T_1$  and verify that  $T_1$  axes are parallel to  $T_2$  axes (two vectors  $\vec{a}$  and  $\vec{b}$  are parallel if  $a_i = kb_i$ , i = 1, 2, 3).

Moving axes parallelism is discussed in sect. 2. It is shown in sect. 3 that the notion is needed not only for the boost definition but also for refinement of the general Lorentz transformation definition.

Section 4 demonstrates that the property of the parallelism of the Lorentz triads is nontransitive (unlike the case of immovable triads), i.e., if  $T_1 \parallel T_2$  and  $T_2 \parallel T_3$ , then  $T_1$  is not parallel to  $T_3$  in the general case. This is directly related to the well-known property of boosts: They do not form a group, i.e., the product  $B_2B_1$  of two boosts is not a boost B in general. Instead,  $B_2B_1$  is equal to a boost multiplied by a space rotation R:  $B_2B_1 = RB$  e.g., see the books [1] and [2]. Two names are used for R in the literature: Thomas rotation or Wigner rotation (apropos of the terminology, see e.g. [3],[4]). I shall use the appellation "Thomas-Wigner rotation".

Physical applications of the rotation cannot be understood if transitivity property of Lorenz triads' parallelism is unconsciously assumed. This is illustrated in sect. 5 using as examples the Thomas precession and relativistic phase analysis for spinning particle scattering. The rotation is also known to be of importance when measuring the abnormal electron and muon magnetic moments, see e.g.[5].

The summary is given in the concluding section 6.

## 2 PARALLELISM OF LORENTZ FRAMES' TRIADS

As usual, it is supposed that in each Lorentz frame there are synchronized clocks, rulers, radars and other devices which allow one to measure lengths, angles and velocities. The information interchange between  $S_1$  and  $S_2$  (e.g. by radio or light signals) is also assumed to be possible.

### 2.1 Definition of moving triads parallelism

Fisher [6] emphasized the necessity of a particular definition of triads' parallelism and proposed the following one. An observer in  $S_1$  measures the projections  $(v_{21})_i$ i = 1, 2, 3 of the  $S_2$  velocity relative to  $S_1$  (with respect to his triad  $T_1$ ). The projections  $(v_{12})_i$  of the  $S_1$  velocity relative to  $S_2$  (with respect to  $T_2$ ) are measured in  $S_2$ . The  $S_1$  observer informs the  $S_2$  observer of his results. Fisher proposed to consider  $T_2$  being parallel to  $T_1$  if

$$(v_{21})_i = (-v_{12})_i, \quad i = 1, 2, 3 \quad or \quad \theta_i^{(1)} = \theta_i^{(2)}$$
 (1)

where  $\theta_i^{(1)}$  are the angles between the  $\vec{v}_{21}$  and triad  $T_1$  axes  $\vec{e}_i^{(1)}$  and  $\theta_i^{(2)}$  are the angles between  $-\vec{v}_{12}$  and  $\vec{e}_i^{(2)}$ .

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Obviously, the triads are not parallel if eq.(1) does not hold, i.e., it is a necessary condition for the triads' parallelism. But I stress that it is not a sufficient one. Indeed, eqs.(1) survive if one rotates arbitrarily  $T_1$  around  $\vec{v}_{21}$  or  $T_2$  around  $\vec{v}_{12}$ . This is evident if one considers the equivalent rotation of a vector with respect to invariable axes. The vector does not change when rotating around itself. One may also use the formula for rotation around a direction  $\vec{n}$  at an angle  $\alpha$ :

$$\vec{a}' = \vec{a} + \vec{n} \times \vec{a} \sin \alpha + [\vec{n}(\vec{n}\vec{a}) - \vec{a}](1 - \cos \alpha).$$
<sup>(2)</sup>

If  $\vec{n} = \vec{a}/a$ , then  $a'_i = a_i$ . Therefore Fisher's proposal needs a complement.

Note that Fisher proposed a check of the  $T_1$  and  $T_2$  parallelism. I shall at first consider a construction of the  $T_2$  triad which can be regarded as being parallel to  $T_1$ . Measurements or observations, which may be performed in the frames  $S_1$  and  $S_2$ , will be used for the construction. Relative velocities are the basic supporting observables which can be used following [6].

To construct the needed triple  $\vec{e}_i^{(2)}$ , let us choose in  $S_2$  an auxiliary spherical coordinate system with  $-\vec{v}_{12}$  as an axis z. The polar angles of  $\vec{e}_i^{(2)}$  in this system coincide with the angles  $\theta_i^{(2)}$  which are required to be equal to  $\theta_i^{(1)}$ . Evidently, one has

$$\cos^2 \theta_1 + \cos^2 \theta_2 + \cos^2 \theta_3 = 1, \quad \theta_i = \theta_i^{(1)} \quad or \quad \theta_i^{(2)}.$$
 (3)

In order to construct  $\vec{e}_i^{(2)}$ , one must know in addition to  $\theta_i$  the azimuthes  $\varphi_i$  of  $\vec{e}_i^{(2)}$ . Note that the needed  $\vec{e}_i^{(2)}$  must be mutually orthogonal

$$(\vec{e}_i^{(2)} \cdot \vec{e}_j^{(2)}) = \cos\theta_i \cos\theta_j + \sin\theta_i \sin\theta_j \cos(\varphi_i - \varphi_j), \quad \forall i \neq j$$
(4)

One can show that the differences  $\varphi_2 - \varphi_1, \varphi_3 - \varphi_1$  (and consequently  $\varphi_3 - \varphi_2 = (\varphi_3 - \varphi_1) - (\varphi_2 - \varphi_1)$  are fixed by eqs. (4) ( $\theta_i$  being given) together with eq. (3) and by the requirement that  $\vec{e}_1^{(2)}, \vec{e}_2^{(2)}, \vec{e}_3^{(2)}$  should form the right-hand triple (as  $\vec{e}_i^{(1)}$  do). Only these differences are fixed but not the very azimuthes  $\varphi_1, \varphi_2, \varphi_3$ , e.g.,  $\varphi_1$  may be arbitrary. This arbitrariness has been discussed above when criticizing Fisher's proposal. So the given angles  $\theta_i$  allow one to construct continually many triples  $\vec{e}_i^{(2)}$ . To complete the construction of the needed (parallel to  $T_1$ ) triple, one must fix any of the azimuthes, e.g.  $\varphi_1$ .

I shall outline the following example of a measuring device which allows doing this. Let us take a luminous rod which represents the vector  $\vec{e}_1^{(1)}$  of the triad  $T_1$ .



The observer  $S_2$  photographes it using a camera which is at the  $S_2$  origin. Its optical axis is directed along  $\vec{v}_{12}$  the photographic plate being orthogonal to  $\vec{v}_{12}$ . So a line (segment) is obtained on the plate which is the image of the (moving) rod  $\vec{e}_1^{(1)}$ , see the dashed line on Fig. 1.



Fig. 1. Boldface dot represents the  $S_2$  origin. The dashed line is the image of  $\vec{e}_1^{(1)}$  on a photographic plate (shown by the circle).

The image and the optical axis determine a plane  $\prod_1$ . A unit length vector is constructed which is in  $\prod_1$  and makes the angle  $\theta_1$  with  $(-\vec{v}_{12})^{-1}$ . This vector is declared (defined) to be the axis  $\vec{e}_1^{(2)}$  which is parallel to  $\vec{e}_1^{(1)}$ .

Let us make some subsidiary notes. We suppose that at  $t_1 = t_2 = 0$  the origins of  $T_1$  and  $T_2$  coincide and the velocity of  $S_1$  origin observed from  $S_2$  origin is represented by the same vector  $\vec{v}_{12}$  at all times ( $\vec{v}_{12}$  does not depend on time). This means that one deals with a pure Lorentz transform but not with its combination with a translation.

The moment of photographing and the time of exposure are inessential.

The image given by the camera is not inverted or rotated (about the optical axis) as compared to its prototype. This may be verified in a separate experiment performed in  $S_2$ .

Of course, instead of the suggested  $T_2$  construction one may check the  $T_1$  and  $T_2$  parallelism. The observer  $S_2$  finds the plane  $\prod_1$  and verifies that  $\vec{e}_1^{(2)}$  is in the plane and makes the angle  $\theta_1$  with  $(-\vec{v}_{12})$  which is equal to the angle between  $\vec{e}_1^{(1)}$  and  $\vec{v}_{21}$ , etc.

<u>Remark</u>. The proposed definition of the triads' parallelism is valid for both the finite limiting (invariant) velocity (Lorentz case) and the infinite one (Galilei case). The definition allows one to obtain, in the usual manner, the Lorentz boosts in the former case and Galilei transformation in the latter case (e.g., see [2]).

The suggested construction of  $T_2 \parallel T_1$  can be applied to the case when  $T_2$  is at rest relative to  $T_1$  but is translated by a vector  $\vec{R}$ . To this end one can treat  $\vec{R}$ 

in the same way as the vector of relative velocity has been considered above. The construction can be used if there are difficulties in simple measuring of all projections of  $\vec{e}_1^{(2)}, \vec{e}_2^{(2)}, \vec{e}_3^{(2)}$  with respect to  $T_1$  (see Introduction).

### 2.2 Other variants of the definition of parallelism

Measuring the photographic images of  $\vec{e}_2^{(1)}$  and  $\vec{e}_3^{(1)}$ , one can obtain the planes  $\prod_2$  and  $\prod_3$  in the same way as  $\prod_1$  has been determined above. Note that the angles between the planes  $\prod_1, \prod_2, \prod_3$  are equal to the differences of azimuthes  $\varphi_1^{(2)}, \varphi_2^{(2)}, \varphi_3^{(2)}$  of  $\vec{e}_i^{(2)}$ . Indeed, one may define  $\varphi_i^{(2)}$  as the angle between the plane  $\prod_1$  and an arbitrary plane containing the line connecting the  $S_1$  and  $S_2$  origins (it is directed along  $\vec{v}_{12}$ ). Let us emphasize that measuring  $\prod_2$  and  $\prod_3$  in addition to  $\prod_1$  is excessive (i.e., it would give no new information) if all polar angles  $\theta_i$  of  $\vec{e}_i^{(2)}$  are known. Indeed, the differences  $\varphi_i - \varphi_j$  of the angles between the planes  $\prod_1$  are fixed if  $\theta_i$  are given, see the text below eq.(4).

But one can construct  $T_2 \parallel T_1$  using chiefly the azimuthes  $\varphi_1^{(2)}, \varphi_2^{(2)}, \varphi_3^{(2)}$  (measured with the help of the planes  $\prod_1, \prod_2, \prod_3$ ) instead of  $\theta_1, \theta_2, \theta_3$  and  $\varphi_1^{(2)}$ . It is possible to show, using eq. (4), that  $\theta_i^{(2)}$  are determined by  $\varphi_2^{(2)} - \varphi_1^{(2)}$  and  $\varphi_3^{(2)} - \varphi_1^{(2)}$  if one knows in addition whether  $\theta_1$  (or  $\theta_2$  or  $\theta_3$ ) is either acute or obtuse (note that  $0 \le \theta_i \le \pi$ ).

Besides the two stated ways of defining parallelism let us indicate the third one. It uses the particular case when the axis  $\vec{e}_1^{(1)}$  of  $T_1$  is chosen along  $\vec{v}_{21}$ . Then, the axis  $\vec{e}_1^{(2)}$  of  $T_2$  must be directed along  $(-\vec{v}_{12})$ . The directions of other axes  $\vec{e}_2^{(2)}$  and  $\vec{e}_3^{(2)}$  are determined as stated above, e.g.  $\vec{e}_2^{(2)}$  must be directed in the plane  $\prod_2$  along  $\vec{e}_2^{(1)}$  image (in this case  $\theta_2 = \pi/2$ ). The general case can be reduced to this particular one. To ascertain that  $T_1$  and  $T_2$  are parallel, both triads  $T_1$  and  $T_2$  must be rotated so that their new x-axis would coincide with the direction of the relative velocity (i.e.,  $\vec{v}_{21}$  for  $T_1$  and  $-\vec{v}_{12}$  for  $T_2$ ). If these rotations are equal (more exactly if they differ only by rotations around relative velocity), then further verification of the parallelism proceeds as in the particular case above. If they are not, then  $T_1$  is not parallel to  $T_2$ .

<u>Remark 1</u>. Aharoni [2] at the beginning of his ch. 1.11 discussed the triad parallelism. In distinction to my approach, he did not strive for a definition which would precede Lorentz transformation derivation. But he pointed out that the parallelism in the general case can be reduced to the parallelism in the case when the relative velocity is parallel to the x-axis.

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<u>Remark 2</u>. The difficulty of the parallelism definition may be illustrated when discussing the following simple suggestion: " $T_1$  and  $T_2$  are parallel if they coincide when the origins of  $S_1$  and  $S_2$  coincide". It is implied that the coincidence is detected in any of the frames, e.g., in  $S_1$ . The  $S_1$  triad  $T_1$  must coincide with an image of  $T_2$ which is to be measured in  $S_1$ . For example,  $T_2$  can be a triple of mutually orthogonal

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<sup>&</sup>lt;sup>1</sup>The described device does not measure  $\theta_1$ , of course. The numerical value of  $\theta_1$  is communicated from  $S_1$  to  $S_2$  by radio. There exist two possible vectors in  $\prod_1$  having the same angle  $\theta_1$  with  $(-\vec{v}_{12})$ . The right vector makes an acute angle with the image if  $\vec{e}_1^{(1)}$ 

rods, and the measurement can be exemplified by the device for detecting moving rod lengths. In the Lorentz case, the image of  $T_2$  turns out to be, in general, a triple of vectors which are not mutually orthogonal. Such a triple cannot coincide with the triad  $T_1$ , and the suggestion fails.

# 3 LORENTZ FRAMES' PARALLELISM AND DETERMINATION OF THE GENERAL LORENTZ TRANSFORMATION

As has been stated above, the definition of the triad parallelism must precede the boost determination. Let us show that the definition allows us also to refine upon the definition of the general Lorentz transformation (GLT) when the triads  $T_1$  and  $T_2$  are not parallel.

The boost matrix depends on three parameters, viz. the projections of relative velocity. One usually says that the GLT matrix depends, in addition, on three Euler rotation angles. But the triad  $T_2$  moves relative to  $T_1$  while the Euler angles determine the mutual orientation of two immovable triads. The following refinement of the GLT angles is proposed. In the Lorentz frame  $S_2$ , the triad  $T_2^{\parallel}$  parallel to  $T_1$  is constructed in the manner explained in subsect. 2.1. The triads  $T_2^{\parallel}$  and  $T_2$ are mutually immovable, and there are Euler rotations which turn  $T_2^{\parallel}$  into  $T_2$ . The angles of these rotations can be taken as GLT parameters. Of course, one can define the latter using the rotation which turns the triad  $T_1$  into the triad  $T_1^{\parallel}$  which is parallel to  $T_2$ .

Let  $r_i^{(2)}$  denote space coordinates of an event relative to  $T_2^{\parallel}$ , and  $\rho_i^{(2)}$  are the event coordinates relative to  $T_2$ . We have

$$r_i^{(2)} = \sum_j \mathcal{D}_{ij} \rho_j^{(2)} \quad or \quad \vec{r}^{(2)} = \mathcal{D} \vec{\rho}^{(2)} \tag{5}$$

where  $\mathcal{D}$  is the matrix of the rotation which turns  $T_2^{\parallel}$  into  $T_2$ . As  $T_2^{\parallel} \parallel T_1$  the coordinates  $(r_i^{(2)}, t^{(2)})$  of the event are expressed in terms of its coordinates  $(r_i^{(1)}, t^{(1)})$  relative to  $S_1$  with the help of a boost (for the boost matrix derivation see e.g. [1],[2])

$$\vec{r}^{(2)} = \vec{r}^{(1)} + \vec{v}_{21}(\vec{r}^{(1)} \cdot \vec{v}_{21})(\gamma_{21} - 1)/v_{21}^2 - \vec{v}_{21}\gamma_{21}t^{(1)}$$

$$\vec{v}^{(2)} = \gamma_{21}[t^{(1)} - (\vec{r}^{(1)} \cdot \vec{v}_{21})/c^2], \quad \gamma_{21} \equiv [1 - v_{21}^2/c^2]^{-1/2}$$
(6)

It follows from eqs.(3) and (4) that

$$\vec{\rho}^{(2)} = \mathcal{D}^{-1}\vec{r}^{(2)} = \mathcal{D}^{-1}\vec{r}^{(1)} + \mathcal{D}^{-1}\vec{v}_{21}(\vec{r}^{(1)}\cdot\vec{v}_{21})(\gamma_{21}-1)/v_{21}^2 - \mathcal{D}^{-1}\vec{v}_{21}\gamma_{21}t^{(1)};$$

$$t^{(2)} = \gamma_{21}[t^{(1)} - (\vec{r}^{(1)}\vec{v}_{21})/c^2] ,$$
(7)

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So GLT is represented as a product of a boost and a rotation.

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Möller [1] gives another writing of eq.(7). If  $\vec{v}_{21}$  is  $S_2$  velocity relative to  $S_1$  (the projections of  $\vec{v}_{21}$  or  $T_1$  are implied), then  $-\vec{v}_{21}$  is  $S_1$  velocity relative to  $T_2^{||}$ . The velocity  $\vec{v}_{12}$  of  $S_1$  relative to  $T_2$  is connected with  $-\vec{v}_{21}$  by the rotation

$$-\vec{v}_{21} = \mathcal{D}\vec{v}_{12} \quad or \quad \vec{v}_{12} = -\mathcal{D}^{-1}\vec{v}_{21}.$$
(8)

(9)

Using eq. (8), one can rewrite eq.(7) in the form of eq. (2.28b) from [1]

$$\vec{\rho}^{(2)} = \mathcal{D}^{-1}\vec{r}^{(1)} - \vec{v}_{12}(\vec{r}^{(1)} \cdot \vec{v}_{21})(\gamma_{21} - 1)/\vec{v}_{21}^2 - \vec{v}_{12}\gamma_{21}t^{(1)}$$
$$t^{(2)} = \gamma_{21}[t^{(1)} - (\vec{r}^{(1)} \cdot \vec{v}_{21})/c^2].$$

## 4 NONTRANSITIVITY OF THE LORENTZ TRIADS' PARALLELISM AND THOMAS - WIGNER ROTATION

The property "if a = b and b = c then a = c" may serve as an example of the notion of transitivity. The equality of elements a, b and c and can be replaced by other binary relations, e.g., by the property of being parallel in the case when a, b and care vectors. It is natural to ask whether the binary relation "Lorentz triads  $T_1$  and  $T_2$  are parallel" is transitive, i.e., is it true "if  $T_1 \parallel T_2$  and  $T_2 \parallel T_3$  then  $T_1 \parallel T_3$ "? Of course, if one draws on a sheet of paper these three triads, as one usually does it (see, e.g., Figure 2), then all triads turn out to be parallel pairwise. But really we ascertain in this manner that this is the property of immovable triads. It will be shown in this section that triads' parallelism (defined above in sect. 2) has no transitive property when invariant (limiting) velocity is finite (the Lorentz case).

### 4.1 Nontransitivity of the Lorentz triads parallelism

The nontransitivity results from the following reasoning. If  $T_1 \parallel T_2$ , then the transformation from  $S_1$  to  $S_2$  is a boost  $B_{21}$ . If  $T_2 \parallel T_3$ , then the transformation  $S_3 \leftarrow S_2$ is also a boost  $B_{32}$ . If  $T_1 \parallel T_3$ , then the transformation  $S_3 \leftarrow S_1$  must also be a boost according to the boost definition, see Introduction (1). However, the transformation  $S_3 \leftarrow S_1$  may be determined as the product  $B_{32}B_{21}$ . It is not difficult to show that the product is not a boost in the general case, e.g., see [1],[2]. So  $T_1$  cannot be parallel to  $T_3$ , and transitivity does not hold.

Let us demonstrate using the following simple example [2], that  $B_{32}B_{21}$  is not a boost. Let  $B_{21}$  be the boost with the relative velocity  $\vec{v}_{21} \parallel \vec{e}_x^{(1)}$  and  $B_{32}$  be the boost with  $\vec{v}_{32} \parallel \vec{e}_y^{(2)}$ , see Fig. 2.

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Using eq. (6) we can write the matrices  $B_{32}$  and  $B_{21}$ , calculate their product  $B_{32}B_{21}$  and compare it with the matrix of a boost *B* corresponding to a velocity  $\vec{v}$ , see again eq. (6). It turns out that presupposed equalities of the matrix elements  $(B_{32}B_{21})_{\mu\nu}$  and  $B_{\mu\nu}$ ,  $\mu, \nu = 1, 2, 3, 0$  are mutually exclusive. In particular, the equality of the last columns of  $B_{32}B_{21}$  (i.e., elements  $\mu, 0$ ) give some values for  $v_x, v_y$  while the equality of the last row (i.e., elements  $0, \mu$ ) gives differing values for  $v_x, v_y$ .

A simpler proof of the nontransitivity is given in [1]. Suppose that  $T_1 \parallel T_3$  along with  $T_1 \parallel T_2$  and  $T_2 \parallel T_3$ . Then the projection of the velocity  $\vec{v}_{31}$  of  $S_3$  relative to  $S_1$  and of the velocity  $\vec{v}_{13}$  of  $S_1$  relative to  $S_3$  must satisfy

$$(\vec{v}_{31}) = -(\vec{v}_{13})_i, \quad i = 1, 2, 3.$$
 (10)

See subsect. 2.1, eq.(1). I remind that  $(\vec{v}_{31})_i$  are projections onto  $T_1$  while  $(v_{13})_i$  are projections onto  $T_3$ . Both the velocities  $\vec{v}_{31}$  and  $\vec{v}_{13}$  can be computed as functions of  $\vec{v}_{21}$  and  $\vec{v}_{32}$ . For example the velocity  $\vec{v}_{31}$  of  $S_3$  relative to  $S_1$  can be determined with the help of the boost  $B_{21}$  (the corresponding velocity being  $\vec{v}_{21}$ ) and the velocity  $\vec{v}_{32}$  of  $S_3$  relative to  $S_2$ , e.g. see [1] ch. 2.7, eq. (2.55). Let us record the result as  $\vec{v}_{31} = s(\vec{v}_{32}/\vec{v}_{21})$ , for explicit expression see [1], eq. (2.55). Analogously  $\vec{v}_{13}$  can be determined as

$$\vec{v}_{13} = s(\vec{v}_{12}/\vec{v}_{23}) = s(-\vec{v}_{21}/-\vec{v}_{32}) \tag{11}$$

see [1], eq. (2.55'). It turns out that eq. (10) does not hold in general. This means that the triads  $T_1$  and  $T_3$  are not parallel.

<u>Note</u>. The function  $s(\vec{v}/\vec{v}')$  is referred usually to as "sum of  $\vec{v}$  and  $\vec{v}'$ )". This name seems to be inappropriate in the general case because  $s(\vec{v}/\vec{v}')$  depends upon  $\vec{v}$  and  $\vec{v}'$  in different ways and does not have the property  $s(\vec{v}/\vec{v}') = s(\vec{v}'/\vec{v})$  except for the case  $\vec{v} \parallel \vec{v}'$ .

### 4.2 Thomas-Wigner rotation as the measure of the difference of $T_1$ vs. $T_3$ orientations

Let us consider quantitative difference of the  $T_1$  and  $T_3$  orientations provided that  $T_1 \parallel T_2$  and  $T_2 \parallel T_3$ .

Lorentz transformations form a group; therefore, the product  $B_{32}B_{21}$  of two boosts is generally speaking a GLT i.e., the product RB of a boost B and of a rotation R, see sect. 3. Here, R denotes the  $4 \times 4$  matrix such that its time-space and space-time elements are zero, time-time element is unity and space-space elements form a  $3 \times 3$  rotation matrix, see sect. 3. The parameters of B and R must be determined from the equation

$$B_{32}B_{21} = RB. (12)$$

This is a hard algebraic work, which has been carried out, e.g., see [7]-[11]. It turns out that the boost B velocity is equal to  $\vec{v}_{31} = s(\vec{v}_{32}/\vec{v}_{21})$ . The rotation R is



Fig. 2. The sequence of two boosts with nonparallel relative velocities  $\vec{v}_{21}$  and  $\vec{v}_{32}$ .



Fig. 3. Succession of boosts connecting the particle c rest systems  $S_{II}$  and  $S_{I}$ . Y-axes of all Lorentz frames are perpendicular to the plane of Fig. The axes  $x_{II}$  and  $z_{II}$  of  $S_{II}$  are drawn by the solid lines; the dashed lines show the  $S_I$  axes  $x_I$  and  $z_I$ . also determined as a function of  $\vec{v}_{32}$  and  $\vec{v}_{21}$ ; R is called here the Thomas-Wigner rotation, see Introduction.

Being the boost, *B* must transform from the Lorentz frame  $S_1$ , into the frame  $S_3^{\parallel}$  whose triad is parallel to  $T_1$  ( $S_3^{\parallel}$  velocity relative to  $S_1$  being equal to  $\vec{v}_{31}$ ). The triad has been denoted earlier as  $T_3^{\parallel}$ . So the space-space part of *R* must be the rotation which turns  $T_3^{\parallel}$  into  $T_3$  thereby determining the latter

$$T_2 = RT_3^{\parallel} \quad or \quad T_3 = RT_1.$$
 (13)

We see that the Thomas-Wigner rotation specifies the  $T_3$  orientation relative to  $T_1$  provided that  $T_1 \parallel T_2$  and  $T_2 \parallel T_3$ .

R allows as to express  $(-\vec{v}_{13})_j$ , j = 1, 2, 3  $(-\vec{v}_{13} \text{ projections on } T_3)$  in terms of  $(v_{31})_i$ , i = 1, 2, 3 (projections on  $T_1$ )

$$-\vec{v}_{13})_j = \Sigma_i (R^{-1})_{ji} (\vec{v}_{31})_i \quad or \quad \vec{v}_{31} = R(-\vec{v}_{13}).$$
<sup>(14)</sup>

Vice versa, if  $(\vec{v}_{31})_i$  and  $\vec{v}_{13})_j$  are given, then one can find the simplest notation  $R_{sim}$  which satisfies eq.(14): the  $R_{sim}$  axis  $\vec{n}$  is parallel to the vector product  $\vec{v}_{31} \times \vec{v}_{13}$  (which is parallel to  $\vec{v}_{31} \times \vec{v}_{21}$ ) and the  $R_{sim}$  angle  $\alpha$  is such that

$$\sin lpha = ec{v}_{31} imes ec{v}_{13} / |ec{v}_{31}|| |ec{v}_{13}||.$$

See eq. (2).

Möller in his ch. (2.8) identifies R with  $R_{sim}$ . However, their equality is not evident because R might differ from  $R_{sim}$  by additional rotations around the vectors  $\vec{v}_{31}$  or  $\vec{v}_{13}$  (the rotation around  $\vec{v}_{31}$  does not change  $\vec{v}_{31}$ ). Nevertheless, actually the rotation R determined by eq. (10) does coincide with  $R_{sim}$ .

One can obtain from eq. (12) its following modification

$$B_{31}B_{21} = B(s(\vec{v}_{21}/\vec{v}_{32}))R = B(-\vec{v}_{13})R,$$
(15)

see eq. (14a) in [9].

## 5 EXAMPLES OF PHYSICAL APPLICATIONS

#### 5.1 Kinematic origin of the Thomas precession

Consider an electron which moves with acceleration in the laboratory system (e.g., in the Coulomb field of a nucleus). Let us introduce the non inertial frame of reference A (Accelerated frame) which moves together with the electron so that the electron at each moment of time is at rest in A. Assume that the A triad  $T(\tau)$  at the moment  $\tau$  is parallel to the A triad  $T(\tau + d\tau)$  at the infinitesimal close moment  $\tau + d\tau$  (A can be called accompanying frame of reference).

Remember that we deal with inertial systems when considering the Thomas-Wigner rotation. To apply this consideration to the case of an accelerated electron, let us introduce a set of inertial frames  $S(\tau), -\infty < \tau < \infty$  such that at each moment  $\tau$  one frame of the set coincides with  $A(\tau)$ . In the case of classical electron, one may assume that its own instantaneous inertial Lorentz frame is introduced at each point of the electron trajectory.

Let us consider two inertial frames  $S_2 = S(\tau_2)$  and  $S_3 = S(\tau_3)$ ,  $\tau_3 = \tau_2 + d\tau$ . According to the A and  $S(\tau)$  definitions, the triads of  $S_2$  and  $S_3$  are parallel. I may refer to Fig. 2 where  $S_1$  denotes the laboratory frame whose axes are parallel to those of  $S_2$ . The evident reservation is that the electron velocity increment  $\vec{v}_{32} = \vec{v}(\tau_3) - \vec{v}(\tau_2)$  is now infinitesimally-small and need not be perpendicular to  $\vec{v}(t_2)$ .

Suppose that the force acting on the electron is torqueless so that the electron spin direction is the same relative to the triads  $T_2$  and  $T_3$  (in the non inertial system A, the spin does not rotate). In the quantum case, the "spin direction" is defined as a mean value of the spin vector operator (the polarization vector). Under the described conditions the Thomas-Wigner rotation means that the triads  $T_1$  and  $T_3$ orientations are different. The electron polarization vector is the same relative to  $T_2$ and  $T_3$  but it has different projections with respect to the laboratory triad  $T_1$  at the times  $\tau_2$  and  $\tau_3$ . This is the origin of the Thomas precession. For its quantitative description and physical significance see, e.g., [12] and [2] and references therein.

### 5.2 The Thomas-Wigner rotation and phase analysis

Let us consider a reaction  $a + b \rightarrow c + d$  (reaction I) involving particles with spins. Its phase analysis requires not only differential cross section measurement but also information on particle polarizations. In particular, one needs to measure the particle c polarization. Let its spin be equal to 1/2. The polarization vector may be determined by measuring angular asymmetries in another reaction II which may be scattering: the particle c scatters on a target  $e: c + e \rightarrow c + e$ . I am going to show that c polarization measured in II cannot be used immediately for the phase analysis of the first reaction I: the polarization vector must be transformed beforehand in a specific manner.

The phase analysis is simplified if one uses the following way of describing the state of the spin particle. One specifies its linear momentum  $\vec{p}$  along with the spin wave function  $\chi_m$  in the particle rest system (and not in the Lorentz system where particle momentum is  $\vec{p}$ ), m being eigenvalues of the projection of the spin vector operator  $\vec{s}$  along  $\vec{p}$  (helicity). The operator  $\vec{s}$  is defined as the particle total angular momentum in the particle rest system. The orbital part of the momentum is then equal to zero, the total angular momentum being reduced to its spin part. For details see, e.g. [13]-[15]. Particle c polarization vector is defined as the mean value of  $\vec{s}$  in the state  $\chi$ . Just this vector can be determined using the reaction II. The corresponding particle rest system is denoted by  $S_{11}$ . There may be distinct particle rest systems which differ by orientations of their triads. I shall now show that there is one more particle rest system  $S_1$  when considering reactions I and II.

The system  $S_{II}$  is linked with the laboratory system  $S_l$  with the help of the boost with velocity  $\vec{\beta}_c$ , parallel to the particle *c* linear momentum  $\vec{p}_c$  in  $S_l$ . One can obtain another particle rest system starting from  $S_l$ . To this end let us perform first the Lorentz transformation from  $S_l$  to the center-of-mass system S' of the reaction I (the corresponding velocity  $\vec{\beta}_a$  being parallel to the linear momentum  $\vec{p}_a$  of the reaction I incident particle *a*). Further, one transforms from S' to the particle *c* rest system  $S_I$  using the velocity  $\vec{\beta}'$  parallel to the momentum  $p'_c$  of the particle *c* in S'. In order to show that the  $S_I$  triad differs from the  $S_{II}$  triad let us write out the succession of boosts which allows one to pass from  $S_{II}$  to  $S_I$ :

1)  $B(S_l \leftarrow S_{II}; -\vec{\beta_c}); -\vec{\beta_c}$  is the  $S_l$  velocity relative to  $S_{II}, \vec{\beta_c} \parallel \vec{p_c}$ .

2) 
$$B(S \leftarrow S_l; \beta_a); \beta_a \parallel p_a$$

3)  $B(S_I \leftarrow S'; \beta')$ .

The corresponding velocity  $\vec{\beta}' \parallel \vec{p}'_c$  is determined by the velocities  $\vec{\beta}_c$  and  $\vec{\beta}_a$ . Indeed,  $\vec{\beta}' = s(\vec{\beta}_c/-\vec{\beta}_a)$ ,  $\vec{\beta}_c$  being the particle *c* velocity with respect to  $S_l$  and  $-\vec{\beta}_a$  being the velocity of  $S_l$  with respect to S', see subsect. 4.1. Let us note that it is the velocities  $\vec{\beta}_c$  and  $\vec{\beta}_a$  (or momenta  $\vec{p}_c$  and  $\vec{p}_a$ ) which are measured directly; the velocity  $\vec{\beta}'$  is to be computed using the former ones. The product

$$B(\vec{\beta}')B(\vec{\beta}_a)B(-\vec{\beta}_c) \tag{16}$$

of the boosts 1), 2), 3) is a rotation. Indeed, let us rewrite eq. (15) as

$$B^{-1}(S(\vec{v}_{21}|v_{32})B(v_{32})B(v_{21}) = R$$
(17)

and compare the l.h.s. of eq. (17) with the product (16) where

$$\vec{\beta}' = s(\vec{\beta}_c/-\vec{\beta}_a) = -s(-\vec{\beta}_c/\vec{\beta}_a)$$
 (18)

Equation (18) can be verified using eq. (2.55) from [1] for the "sum of velocities" s. Being a boost,  $B(\beta')$  satisfies the equation

$$B^{-1}(\vec{\beta}') = B(-\vec{\beta}') \quad or \quad B(\vec{\beta}') = B^{-1}(-\vec{\beta}')$$

Inserting into eq. (16) the equalities  $\vec{v}_{21} = -\vec{\beta}_c$ ;  $\vec{v}_{32} = \vec{\beta}_a$ , we can rewrite the l.h.s. of eq. (17) as the product

$$B^{-1}(s(-\vec{\beta}_{c}/\vec{\beta}_{a}))B(\vec{\beta}_{a})B(-\vec{\beta}_{c}) = B(\vec{\beta}')B(\vec{\beta}_{a})B(-\vec{\beta}_{c})$$
(19)

We see that the product (16) is equal to the Thomas-Wigner rotation R which turns the  $S_{II}$  triad into the  $S_I$  triad. Fig. 3 illustrated the foregoing succession of boosts The polarization vector projections, which can be determined using reaction II, are referred to the  $S_{II}$  triad. Using R, one can calculate the vector projections with respect to the  $S_I$  triad. Just these projections are needed for the reaction I phase analysis.

The rotation R is complementary to the obvious rotation caused by the change of the quantization axes when helicities are used: One must obtain the polarization vector projections on the vector  $\vec{p}'_c$  starting with the polarization vector projections with respect to the direction  $\vec{p}_c$  (and other two axes orthogonal to  $\vec{p}_c$ ).

## 6 CONCLUSION

The construction of parallel moving triads (or verification of their parallelism) meets difficulties which are exemplified by the Remark 2 in subsect. 2.2 and at the beginning of subsect. 2.1.

The measuring and structural methods of the operational definitions of the parallelism are proposed and discussed.

It is shown that the parallelism does not possess the transitivity property when the invariant (limiting) velocity is finite (Lorentz case). This nontransitivity is directly related to the Thomas-Wigner rotation which can be considered as its quantitative measure. Taking the nontransitivity into account is essential when discussing physical applications of the Thomas-Wigner rotation.

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