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ON THE THEORY OF STRUCTURAL PHASE TRANSITIONS IN RbCaF₃



1. INTRODUCTION

Transitions caused by condensation of zone boundary modes associated with rotation of BX_6 octahedra occur in a number of perovskites ABX_3 . It is well established that these phase transitions are caused by the condensation of one or two normal modes and these transform like irreducible representations R_{25} and M_3 . These both modes represent the rotational vibrations of BX_6 octahedra around cubic principal axes. The difference between R_{25} and M_3 is that the R_{25} represents the opposite rotation of the neighbouring BX_6 octahedra along the rotation axis, whereas the M_3 represents the rotations in the same direction.

One can find examples of these transitions in refs.^{1,2'}. Neutron and X-ray structure determinations ^{3'} have shown, that for the phases which have two or more octahedral rotations the static displacements of the ions cannot be accounted for by the linear superposition of R- and M-type rotational modes alone. It was suggested in ^{11'} that for phases in which these modes nave condensed, static displacements associated with the normal mode of X-type are also present.

A structural phase transition in the perovskite ABX_3 caused by the condensation of the parallel components of the R- and M-modes with taking into account the displacements of A-ions corresponding to X-mode has been considered in ref.^{4/}.

The purpose of the present paper is to analyze the structural phase transitions in ABX_3 corresponding to the condensation of nonparallel components of R- and M-modes. Such a transition is encountered in $RbCaF_3$, for example.

2. SYMMETRY ANALYSIS

The atomic displacements corresponding to R_{25} and M_3 modes can be described by three-dimensional irreducible representation r_8 (through this paper, the irreducible representations will be labelled in accordance with $^{/5/}$) of the one-component star $\{\vec{k}_{18}\}$ (the R-point of the Brillouin zone, $\vec{k}_R = (\pi/a)(1,1,1)$) and by the one-dimensional irreducible representation r_5 of the three-component star $\{\vec{k}_{11}\}$ (the M-point of the Brillouin zone, $\vec{k}_{1M} = (\pi/a)(0,1,1)$, $\vec{k}_{2M} = (\pi/a)(1,0,1)$, $\vec{k}_{3M} = (\pi/a)(1,1,0)$).

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© Объединенный институт я серных исследований с. 518197 Бультана, 1983 As is shown in paper $^{/1/}$, for phases in which R- and M-modes have condensed, static displacements of A-ions associated with a normal mode with wave vector of the X-point are also present.

In phases, in which the parallel components of the R- and M-modes have condensed ($r_a \neq 0$, $m_a \neq 0$, a = 1,2,3), the displacements of A-ions along the axis a take place and they transform like the one-dimensional irreducible representation r_4 of the three-component star $\{k_{10}\}$ (the X-point of the Brillouin zone $k_{1X} = (\pi/a)$ (1,0,0), $k_{2X} = (\pi/a)$ (0,1,0), $k_{3X} = (\pi/a)(0,0,1)$).

However, if the nonparallel components of R and M condense $(r_a \neq 0, m_\beta \neq 0, a \neq \beta)$, then the A-ions are displaced along the axis of the R-type rotation, and these displacements transform like the two-dimensional irreducible representation r_{10} of the star $\{\vec{k}_{10}\}$. In this case the displacements of X-ions accompanied by the displacements of A-ions under the structural phase transitions may be described by 12-component order parameter:

$$\mathbf{p} = \{ (\mathbf{r}_1, \mathbf{r}_2, \mathbf{r}_3), (\mathbf{m}_1, \mathbf{m}_2, \mathbf{m}_3), (\mathbf{X}_1^y, \mathbf{X}_1^z, \mathbf{X}_2^z, \mathbf{X}_2^x, \mathbf{X}_3^x, \mathbf{X}_3^y) \}.$$

Following Landau's phenomenological theory of the second order phase transition, we expand the free energy of the system in terms of (r_1, r_2, r_3) , (m_1, m_2, m_3) , $(X_1^y, X_1^z, X_2^z, X_2^x, X_3^x, X_3^y)$ up to the fourth order

$$F = F_{0} + a_{1} \sum_{i=1}^{2} r_{i}^{2} + \beta_{i} \sum_{i=1}^{2} r_{i}^{4} + \gamma_{1} \sum_{j\neq j} r_{i}^{2} r_{j}^{2} + + a_{2} \sum_{i=1}^{3} m_{i}^{2} + \beta_{2} \sum_{i=1}^{3} m_{i}^{4} + \gamma_{2} \sum_{i\neq j} m_{i}^{2} m_{j}^{2} + + A_{1} (\sum_{i=1}^{3} r_{i}^{2}) (\sum_{i=1}^{3} m_{i}^{2}) + A_{2} \sum_{i=1}^{3} r_{i}^{2} m_{j}^{2} + + a_{3} \sum_{i\neq j} (X_{i}^{j})^{2} + \delta \sum_{i\neq j} r_{j} m_{i} X_{i}^{j}.$$
(1)

Each term is constructed so that cubic symmetry operations leave it invariant. It is assumed that only temperature dependent coefficients are a_1, a_2 and

$$a_{1} = a_{1}^{\circ} (T - T_{R}^{\circ}), \quad a_{2} = a_{2}^{\circ} (T - T_{M}^{\circ}),$$

where T_R^o , T_M^o are, respectively, the critical temperatures of (r_1, r_2, r_3) and (m_1, m_2, m_3) separately.

The expression (1) differs from the one used to describe the system in which the condensation of R_{25} and M_3 modes takes place through the inclusion of terms in X_1^j .

The equilibrium state at an arbitrary temperature should be determined by the minimization of F with respect to r_i, m_i and X_i^j , in particular

$$\frac{\delta \mathbf{F}}{\delta \mathbf{X}_{i}^{j}} = 2a_{3}\mathbf{X}_{i}^{j} + \delta \mathbf{r}_{j}\mathbf{m}_{i}; \quad \mathbf{X}_{i}^{j} = -\frac{\delta}{2a_{3}}\mathbf{r}_{j}\mathbf{m}_{i}.$$
(2)

So, one can see that a particular set of non-zero components of R- and M-modes determines which of various X_i^j have non-zero values.

3. PHENOMENOLOGY OF RbCaF3

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The expression (1) for the free energy will be now applied to $RbCaF_8$.

Experimental work up to date indicates that it undergoes a series of structural phase transitions: the 193K transition $(O_h^1 cdot D_{4h}^{18})$ induced by the condensation of one of the components of the triply degenerated $R_{25} ext{ mode }^{/6/}$ and the 50K transition $(D_{4h}^{18} cdot D_{2h}^{10})$ induced by the condensation of $M_3 ext{ mode }^{/7/}$. In the phase below 50K the rubidium displacements along |101| are observed $^{/8/}$.

According to Glazer's notation ^{/9/} the successive phases correspond to the following sequence of tilts:

The solution of (1) corresponding to the above tilt system is

$$r_{1}^{2} = r_{3}^{2} = \frac{-2\beta_{2}\alpha_{1} + A_{1}\alpha_{2}}{2\beta_{2}(2\beta_{1} + \gamma_{1}) - 2\tilde{A}_{1}^{2}},$$
 (3a)

$$m_{2}^{2} = \frac{-a_{g}(2\beta_{1} + \gamma_{1}) + 2\tilde{A}_{1}a_{1}}{2\beta_{2}(2\beta_{1} + \gamma_{1}) - 2\tilde{A}_{1}^{2}}, \qquad (3b)$$

$$X_{2}^{2} = -\frac{\delta}{2a_{3}}r_{3}m_{2}$$
, (3c)

$$X_{2}^{x} = -\frac{\delta}{2a_{3}}r_{1}m_{2}$$
, (3d)

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where $\tilde{A_1} = A_1 - \frac{\delta^2}{4a_3} = A_1 - \delta'$. The stability of this phase requires

$$(4\beta_{2} m_{2}^{2} + 2\delta' r_{1}^{2}) [(4\beta_{1} + 2\gamma_{1})r_{1}^{2} + \delta' m_{2}^{2}] - 4\tilde{A}_{1}^{2}r_{1}^{2}m_{2}^{2} > 0, \qquad (4a)$$

$$a_{3} > 0$$
, (4b)

$$(4\beta_1 - 2\gamma_1) \mathfrak{r}_1^2 + \delta' \mathfrak{m}_2^2 > 0.$$
 (4c)

Under the assumption that the structural phase transitions in $RbCaF_3$ are well described by the dynamic model $^{\prime\,10\prime}$, we are led to:

$$\beta_{1} = \beta_{2} , \quad \gamma_{1} = \gamma_{2} ;$$

$$A_{1} = \gamma_{1} , \quad A_{2} = \mathbf{6}\beta_{1} - \gamma_{1} .$$
(5)

If we furthermore take into account that $r_1^2 = m_2^2$, we can rewrite the inequality (4a) in the form

$$-(\delta')^{2} + 6(\beta_{1} + \gamma_{1})\delta' + 2(4\beta_{1}^{2} + 2\beta_{1}\gamma_{1} - \gamma_{1}^{2}) > 0.$$
(6)

It yields together with inequality (4c) the following condition for the coupling constant $\delta^\prime\colon$

$$2(\gamma_1 - 2\beta_1) < \delta' < 3(\beta_1 + \gamma_1) + w,$$
(7)

where $w = (17\beta_1^2 + 22\beta_1 y_1 + 7y_1^2)^{1/2}$.

It should be here noted that by considering only the R- and M-modes in the expression (1), the following stability conditions for the phase ($r_1 = r_3 \neq 0$, $m_2 \neq 0$) are readily obtained

$$\beta_1 > 0 , \qquad (8a)$$

$$4\beta_{1}^{2} - \gamma_{1}^{2} > 0 .$$
 (8b)

If the phase $(r_3 \neq 0)$ is the previous to the phase mentioned above, the following condition should be satisfied additionally

$$2\beta_1 < \gamma_1 . \tag{9}$$

One can see that the set of inequalities (8a)-(8b) is inconsistent with the inequality (9).

To the light of these results it is seen that the displacements of Rb-ions corresponding to X-mode play an important role in stabilization of the observed phases. Comparing the free energies of the neighbouring $(a^a a^c c^-)$ and $(a^a a^+ a^-)$ phases, we obtain the following expression for the critical temperature:

$$T_{M} = \frac{2aT_{R}^{o} + 2bT_{M}^{o} - o(T_{R}^{o} + T_{M}^{o}) - (T_{R}^{o} - T_{M}^{o})\sqrt{c^{2} - 4ab}}{2(a + b - c)}, \quad (10)$$

where

$$a = [\beta_{1} (2\beta_{1} - \gamma_{1}) - \vec{A}_{1}^{2}] (a_{1}^{\circ})^{2},$$

$$b = \beta_{1} (2\beta_{1} + \gamma_{1}) (a_{2}^{\circ})^{2},$$

$$c = 4\vec{A}_{1} \beta_{1} a_{1}^{\circ} a_{2}^{\circ}.$$

It is easy to check that at $T = T_M$ the squares of the order parameters r_1^2 , m_2^2 are nonvanishing, hence this transition is of the first order.

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К теории структурных фазовых переходов в RbCaF

Рассматриваются структурные фазовые переходы в перовските RbCaF₃, индуцированные мягкими модами R₂₅ и M₃. На основе симметрийного анализа получено разложение свободной энергии с учетом сопутствующих переходу D¹⁸ → D¹⁶_{2b} смещений ионов Rb. При анализе условия стабильности фаз, показано, что одновременная конденсация мод R₂₅ и M₃ возможна лишь при определенной величине константы связи ионов Rb с решеткой.

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On the Theory of Structural Phase Transitions in RbCaF,

Structural phase transitions in prevokite $RbCaF_8$ induced by the soft modes R_{25} and M_8 are considered. On the basis of the symmetry analysis a free energy expansion is obtained, where displacements of Rb ions are taken into account. By analyzing the stability conditions, it was shown that soft modes R_{25} and M_8 may condensate simultaneously only for a definite value of Rb-ion coupling with the lattice.

The investigation has been performed at the Laboratory of Theoretical Physics, JINR.

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