

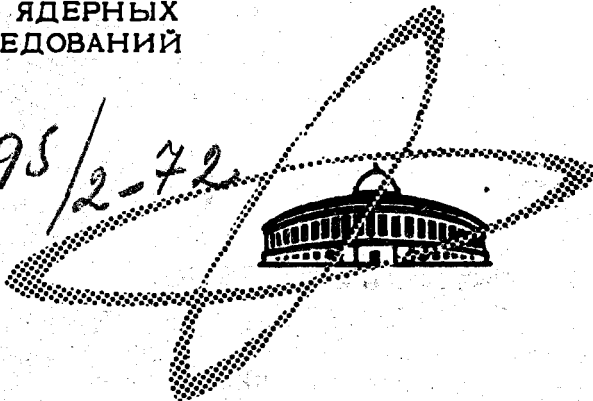
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ОБЪЕДИНЕННЫЙ  
ИНСТИТУТ  
ЯДЕРНЫХ  
ИССЛЕДОВАНИЙ

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E1 - 6613

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ЛАБОРАТОРИЯ ВЫСОКИХ ЭНЕРГИЙ

DIFFERENTIAL CROSS SECTIONS OF THE  
ELASTIC p-p SCATTERING IN THE  
ENERGY RANGE OF 8-70 GEV

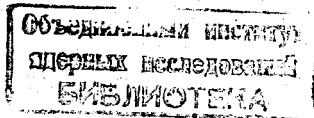
1972

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**DIFFERENTIAL CROSS SECTIONS OF THE  
ELASTIC p-p SCATTERING IN THE  
ENERGY RANGE OF 8-70 GEV**

*Submitted to Nuclear Physics*



## S u m m a r y

In this paper we present the tables of the absolute differential cross-sections of the elastic  $p$ - $p$  scattering together with the values of the slope parameter  $B = \frac{d}{dt} (\ln \frac{d\sigma}{dt})$  and the real part parameter  $a = \frac{\text{Re } A(0)}{\text{Im } A(0)}$  ( $A(0)$  is the amplitude of the elastic  $p$ - $p$  scattering at  $t = 0$ ). The cross section data have been obtained at Serpukhov accelerator over 8 to 70 Gev in the  $t$  - range of  $0.0007 - 0.12(\text{Gev}/c)^2$ .

This paper presents the differential cross sections of the elastic  $p$ - $p$  scattering obtained in two independent sets of measurements.

The experiments have been carried out at the Serpukhov accelerator by the method in which multiple passages of an internal beam of the circular accelerator through a thin target were used. We registered the recoil particles and measured their angle and energy using a system of semiconductor detectors and on-line computer<sup>/1,2/</sup>.

The first part of the measurements covers the momentum transfer squared range of  $0,008 \leq |t| \leq 0,12$  (GeV/c). The method and the results of the measurements of the slope parameter  $B = \frac{d}{dt} (\ln \frac{d\sigma}{dt})$  have been published in ref.<sup>/2/</sup>. One example of differential cross sections of this series is shown in fig. 1.

The second set of the measurements was performed using a gas hydrogen jet as an internal target of the accelerator in the  $t$  - interval of  $0.0007 \leq |t| \leq 0.02$  (GeV/c)<sup>2</sup>. Figure 2 presents the differential cross sections of this series. It is possible to see here the constructive in-

interference effect between Coulomb and nuclear scattering. From this experiment the ratio of the real to the imaginary part of the elastic  $p$ - $p$  scattering amplitude  $a = \frac{Re A(0)}{Im A(0)}$ <sup>3,4/</sup> was determined. The gas target and the equipment used in this experiment are described in ref.<sup>5/</sup>

In both the sets of the measurements the differential cross sections were obtained in relative units. The determination of the absolute elastic  $p$ - $p$  scattering differential cross sections, using the Serpukhov total cross section data<sup>6/</sup>, is described in ref.<sup>4/</sup>

The tables with index\* present the data from the first set only, the tables with\*\* - from the second set of measurements. In those cases when the energy of the primary beam differed not more than by 3 Gev the data of both the sets were joined. These tables are denoted by index\*\*\*.

Figure 3 illustrates the differential cross section in the interval of  $0.001 \leq |t| \leq 0.115$  ( $\text{Gev}^2/c^2$ ).

In front of each table the momentum  $P$  in the lab. system, at which the measurements have been performed, and the values of  $a$  and  $B$  calculated by the Bethe formula<sup>3/</sup>, are given. These values are presented with statistical errors only.

The important sources of the systematic errors are: uncertainty of the sensitive area of semiconductor detectors (which results in a cross section error 1%), the uncertainty of the detector coordinates and apparatus mis-

takes (1%) connected with overloading of the electronics. The root mean square systematic errors are  $\Delta B = \pm 0.3 \text{ (GeV/c)}^{-2}$  and  $\Delta a = \pm 0.028$ .

In the tables\* we use the values of  $a$  from ref.<sup>/4/</sup>. In the set\*\* we take the values of  $B$  from<sup>/2/</sup> (see the note).

The following designations are used in the tables:

$t$  is the square invariant four-momentum transfer in  $(\text{GeV/c})^2$ .  $\frac{d\sigma}{dt}$  is the elastic scattering differential cross section in  $\text{mb}/(\text{GeV/c})^2$ .  $\Delta(\frac{d\sigma}{dt})$  is the absolute statistical error in  $\text{mb}/(\text{GeV/c})^2$ .

The presented tables of the differential cross sections can be used for an analysis of experimental data by different theoretical models.

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Note to the tables: The values of the slope parameter presented at the beginning of each table with index\*, differ insignificantly (within the limit of errors) from those published in ref.<sup>/2/</sup>. This is explained by that the recent data on  $a$ <sup>/4/</sup> and on the  $p$ - $p$  total cross sections<sup>/6/</sup> are used here.

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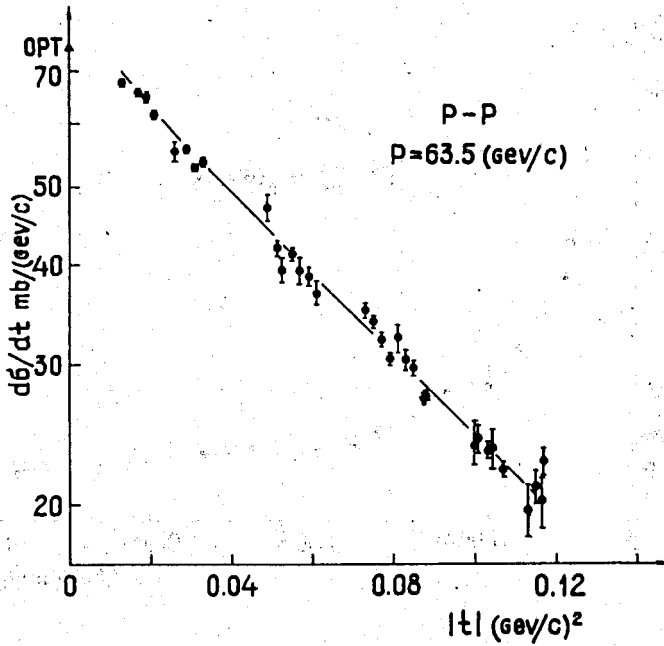


Fig. 1. Differential cross sections of the elastic scattering at  $P = 63.5$  GeV/c ( $0.013 \leq |t| \leq 0.116$  (GeV/c)<sup>2</sup>) (the first series\*).



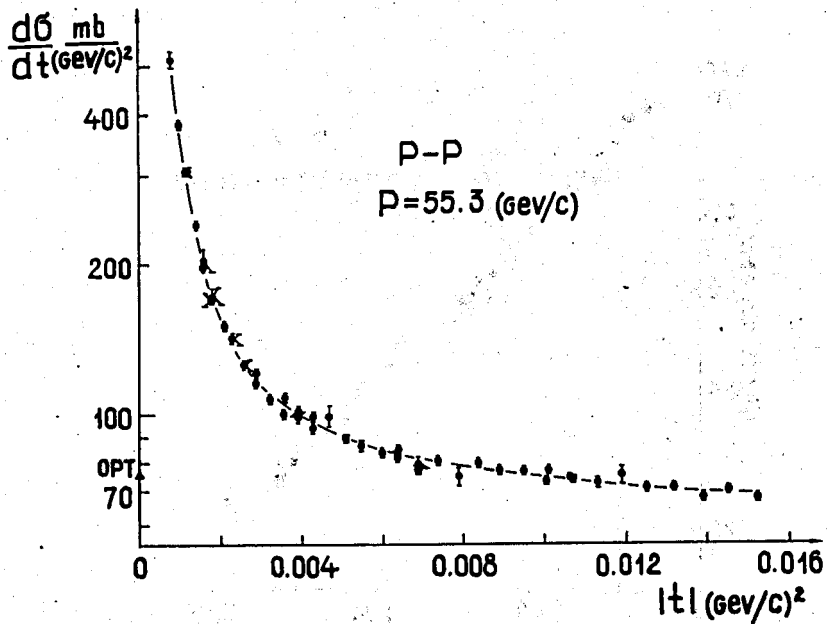


Fig. 2. Differential cross sections of the elastic scattering at 55.4 GeV/c in the interference region ( $0.0008 \leq |t| \leq 0.015$  (GeV/c)<sup>2</sup>) (the second series \*\*).

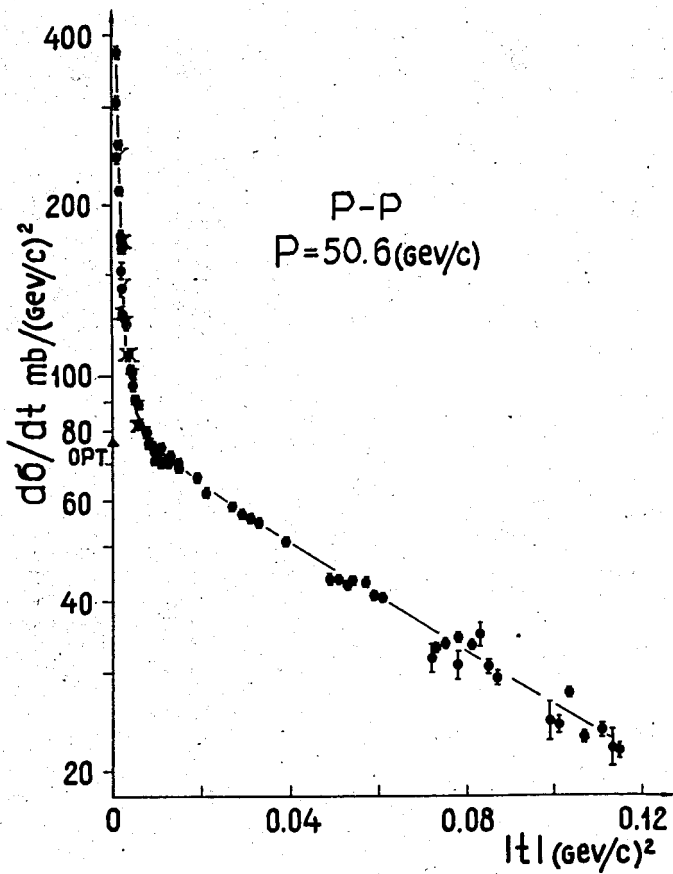


Fig. 3. Differential cross sections of the elastic scattering at  $p = 50.6 \text{ GeV/c}$  ( $0.00096 \leq |t| \leq 0.115 (\text{GeV/c})^2$ ) (the third series\*\*\*).

$$P = 13.15 \text{ eV/c}$$

$$P = 15.526 \text{ eV/c}$$

$$B = 10.52 \pm 0.17 (C/\text{eV}) \cdot \cdot 2$$

$$B = 10.31 \pm 0.15 (C/\text{eV}) \cdot \cdot 2$$

$\sqrt{t}$	$t$	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$	$\sqrt{t}$	$t$	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$
1	0.00900	85.11	1.94	1	0.00890	85.60	1.01
2	0.01141	85.70	1.93	2	0.01109	85.44	1.01
3	0.01353	82.54	1.31	3	0.01044	77.63	0.90
4	0.01541	81.13	1.04	4	0.01906	75.71	1.17
5	0.01713	79.57	1.03	5	0.02663	59.80	2.02
6	0.01913	75.25	1.19	6	0.02859	64.21	1.43
7	0.02070	65.90	1.30	7	0.03053	66.12	1.43
8	0.02204	60.60	1.19	8	0.03635	53.57	3.76
9	0.02450	55.59	1.30	9	0.04632	54.73	2.02
10	0.02700	51.54	1.30	10	0.04830	54.21	2.02
11	0.02893	49.55	1.37	11	0.05032	51.44	1.43
12	0.03100	47.73	1.30	12	0.05303	50.30	1.43
13	0.03340	47.03	1.33	13	0.05617	46.81	2.02
14	0.03500	45.47	1.30	14	0.06739	45.02	1.43
15	0.03683	42.11	1.30	15	0.06925	42.73	2.02
16	0.03971	44.45	1.37	16	0.07116	41.33	1.17
17	0.04357	39.26	1.30	17	0.07263	39.91	1.43
18	0.04747	41.55	1.30	18	0.07557	40.04	2.02
19	0.04930	35.31	1.50	19	0.07600	40.14	2.02
20	0.04953	31.92	1.27	20	0.07963	38.21	0.70
21	0.04964	31.19	1.30	21	0.08078	36.39	0.76
22	0.04410	30.31	1.30	22	0.09487	30.50	2.02
				23	0.09713	30.81	1.17
				24	0.09894	29.41	1.43
				25	0.10249	29.08	1.43
				26	0.10512	28.32	2.02
				27	0.10692	29.68	2.02

P=21.71GEV/C

P=24.56GEV/C

B=10.47+/-0.14(C/GEV)\*\*2

B=10.48+/-0.13(C/GEV)\*\*2

P=21.71GEV/C				P=24.56GEV/C			
N	-t	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$	N	-t	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$
1	0.01495	76.38	0.90	1	0.01085	78.87	1.06
2	0.01671	74.51	0.90	2	0.01515	75.32	0.82
3	0.01857	72.51	1.27	3	0.01691	73.90	0.82
4	0.02017	70.87	1.27	4	0.02042	68.61	1.06
5	0.02724	64.88	0.90	5	0.02759	63.66	0.75
6	0.02960	63.31	1.27	6	0.02948	62.46	1.29
7	0.03160	61.66	1.27	7	0.03099	62.76	1.29
8	0.04778	51.45	1.80	8	0.03215	57.95	1.83
9	0.04982	47.35	1.80	9	0.03781	57.07	0.40
10	0.05158	47.79	1.94	10	0.04891	48.45	1.29
11	0.05293	50.57	1.99	11	0.05030	47.20	1.83
12	0.05488	46.58	1.27	12	0.05230	48.55	0.75
13	0.05793	44.83	1.30	13	0.05523	47.59	1.06
14	0.06972	39.57	1.27	14	0.05647	45.48	1.29
15	0.07188	37.96	1.80	15	0.07044	40.02	1.29
16	0.07242	38.63	1.90	16	0.07267	38.37	1.06
17	0.07462	33.67	0.90	17	0.07547	37.39	0.75
18	0.07792	36.92	1.80	18	0.07921	37.27	1.29
19	0.07888	35.75	1.30	19	0.08341	34.45	0.60
20	0.08110	37.84	1.80	20	0.08410	32.61	0.69
21	0.08301	35.23	0.46	21	0.09696	27.35	1.29
22	0.09563	30.29	1.30	22	0.09666	28.66	1.06
23	0.09631	32.56	1.80	23	0.10009	28.64	1.83
24	0.09879	28.15	1.27	24	0.10277	28.94	0.75
25	0.10145	29.42	1.85	25	0.10678	27.58	1.06
26	0.10219	26.40	1.30	26	0.11089	25.29	1.06
27	0.10549	25.87	1.30				
28	0.10651	27.33	1.30				
29	0.10907	26.98	1.30				
30	0.11922	25.21	1.30				

$$\sqrt{s} = 27.53 \text{ GeV}/c$$

$$\sqrt{s} = 30.45 \text{ GeV}/c$$

$$B = 10.52 + / - 0.12 (C/\text{GeV})^{**2}$$

$$B = 10.49 + / - 0.12 (C/\text{GeV})^{**2}$$

$\sqrt{s}$	$-t$	$\frac{d\sigma}{dt}$	$\Delta\left(\frac{d\sigma}{dt}\right)$	$\sqrt{s}$	$-t$	$\frac{d\sigma}{dt}$	$\Delta\left(\frac{d\sigma}{dt}\right)$
1	0.00929	31.53	0.56	1	0.01101	77.01	0.82
2	0.01094	77.86	1.15	2	0.01889	69.98	0.82
3	0.01234	77.32	1.15	3	0.02787	60.05	0.82
4	0.01524	74.40	0.81	4	0.02883	61.12	0.64
5	0.01705	71.70	0.81	5	0.03075	57.81	1.43
6	0.01877	72.13	1.15	6	0.03239	59.44	1.01
7	0.02059	63.24	1.15	7	0.03837	55.61	0.31
8	0.02972	50.53	1.41	8	0.04927	48.32	1.01
9	0.03126	59.75	1.41	9	0.05069	47.65	0.82
10	0.03240	61.35	1.99	10	0.05307	47.41	0.58
11	0.03812	56.53	0.44	11	0.05567	45.10	1.01
12	0.04861	46.70	1.99	12	0.05678	46.53	1.43
13	0.05054	44.34	1.41	13	0.05911	45.87	0.82
14	0.05273	46.44	0.81	14	0.07146	38.97	1.01
15	0.05532	46.33	1.41	15	0.07319	36.88	0.82
16	0.05640	46.53	1.99	16	0.07411	40.03	1.43
17	0.05894	46.14	1.41	17	0.07657	37.10	0.58
18	0.07134	37.34	1.15	18	0.07966	35.32	1.01
19	0.07326	36.77	1.15	19	0.08097	32.49	1.43
20	0.07581	37.95	1.41	20	0.08373	33.50	0.82
21	0.07622	35.53	1.00	21	0.08515	33.42	0.38
22	0.07917	36.03	1.41	22	0.09873	27.26	0.82
23	0.08043	35.56	1.99	23	0.10098	27.83	0.82
24	0.08319	34.33	1.15	24	0.10396	26.96	1.01
25	0.08451	33.71	0.53	25	0.10441	27.37	0.79
26	0.08773	27.41	1.41	26	0.10783	25.56	1.01
27	0.09934	23.56	1.41	27	0.10931	23.35	1.43
28	0.10050	27.72	1.41	28	0.11193	24.18	1.43
29	0.10360	27.33	0.81	29	0.11277	24.39	1.01
30	0.10716	23.03	1.41				
31	0.10859	24.93	1.99				
32	0.11120	26.77	1.99				
33	0.11207	24.37	1.41				

P=33.32 GEV/C

P=36.16 GEV/C

B=10.69+/-0.12 (C/GEV)\*\*2

B=10.57+/-0.11 (C/GEV)\*\*2

P=33.32 GEV/C				P=36.16 GEV/C			
N	-t	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$	N	-t	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$
1	0.01707	70.41	0.55	1	0.00932	78.71	0.56
2	0.02083	67.38	0.84	2	0.01112	77.14	1.02
3	0.02314	61.40	0.59	3	0.01520	71.00	0.88
4	0.03035	57.22	0.84	4	0.01701	70.69	0.63
5	0.03255	59.39	1.03	5	0.01909	70.63	1.02
6	0.03857	54.47	0.32	6	0.02092	65.55	1.02
7	0.04452	47.48	1.03	7	0.02670	62.94	1.77
8	0.05095	44.86	0.84	8	0.02826	61.35	0.72
9	0.05335	45.14	0.59	9	0.03048	59.49	1.02
10	0.05496	43.17	1.03	10	0.03874	54.39	0.59
11	0.05709	46.13	1.46	11	0.04935	48.03	1.77
12	0.05962	41.40	1.03	12	0.05091	45.82	0.88
13	0.07183	37.77	1.03	13	0.05358	46.05	0.72
14	0.07327	36.57	1.03	14	0.05658	44.40	1.02
15	0.07433	37.17	1.03	15	0.05987	41.90	1.25
16	0.07697	35.02	0.59	16	0.07248	36.78	1.02
17	0.09052	34.15	0.94	17	0.07444	37.66	1.02
18	0.09370	36.10	1.46	18	0.07730	35.88	0.72
19	0.08544	32.82	0.37	19	0.08086	34.84	1.02
20	0.09895	27.06	1.03	20	0.08549	32.42	0.56
21	0.10114	26.75	0.75	21	0.08600	31.38	0.67
22	0.10430	26.19	0.59	22	0.09927	26.90	1.25
23	0.10888	25.54	0.84	23	0.10096	27.11	1.25
24	0.11307	24.38	0.84	24	0.10218	26.28	1.25
				25	0.10525	26.33	0.72
				26	0.10883	25.92	1.25
				27	0.11038	23.81	1.77
				28	0.11355	24.38	1.02

P=45.17GEV/C

P=52.14GEV/C

B=10.90+/-0.09(C/GEV)\*\*2

B=11.00+/-0.12(C/GEV)\*\*2

$N$	$-t$	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$	$N$	$-t$	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$
1	0.01136	72.74	0.56	1	0.01095	71.54	0.84
2	0.01258	72.99	0.81	2	0.01282	70.03	1.03
3	0.01527	70.97	0.57	3	0.01512	69.27	0.78
4	0.01723	68.65	0.43	4	0.01723	66.57	0.65
5	0.02114	64.90	0.72	5	0.01920	67.27	1.83
6	0.02716	59.59	0.72	6	0.02125	65.13	1.20
7	0.02856	57.53	0.51	7	0.02555	58.60	2.07
8	0.03297	55.08	0.93	8	0.02734	58.75	0.93
9	0.05381	44.98	0.81	9	0.02871	58.71	0.73
10	0.05423	44.33	0.61	10	0.03086	57.47	1.03
11	0.05704	42.93	0.81	11	0.03304	54.36	0.93
12	0.05860	40.00	1.14	12	0.03935	51.73	0.45
13	0.06049	40.08	0.93	13	0.04885	46.85	2.07
14	0.07309	34.92	0.81	14	0.05088	44.33	1.20
15	0.07496	35.24	0.66	15	0.05271	44.62	1.20
16	0.07783	33.50	0.66	16	0.05442	43.06	0.84
17	0.07830	33.67	0.72	17	0.05706	39.83	1.46
18	0.08121	33.37	0.93	18	0.05889	39.31	1.46
19	0.08265	33.62	1.14	19	0.06079	40.08	1.46
20	0.08517	30.75	0.66	20	0.07271	34.90	1.03
21	0.08681	30.59	0.35	21	0.07520	34.99	0.93
22	0.10075	26.17	0.72	22	0.07744	34.10	1.46
23	0.10291	25.33	0.72	23	0.07843	32.77	0.78
24	0.10587	25.17	0.93	24	0.08123	32.54	1.20
25	0.10641	24.92	0.57	25	0.08306	32.30	2.07
26	0.10983	24.07	1.14	26	0.08516	31.89	1.03
27	0.11105	23.75	0.93	27	0.08738	29.33	0.45
28	0.11337	22.96	1.61	28	0.10057	25.51	1.20
29	0.11467	22.35	0.72	29	0.10313	24.41	0.93
				30	0.10663	23.49	0.69
				31	0.10948	24.67	2.07
				32	0.11049	23.03	1.46
				33	0.11212	23.46	2.07
				34	0.11499	21.35	1.03

P=54.37GEV/C

P=57.04GEV/C

B=11.12+/-0.13(C/GEV)\*\*2

B=11.11+/-0.19(C/GEV)\*\*2

$\sqrt{s}$	$-t$	$\frac{d\sigma}{dt}$	$\Delta\left(\frac{d\sigma}{dt}\right)$	$\sqrt{s}$	$-t$	$\frac{d\sigma}{dt}$	$\Delta\left(\frac{d\sigma}{dt}\right)$
1	0.01081	75.01	0.34	1	0.01285	69.16	0.75
2	0.01724	66.61	0.65	2	0.01504	69.60	0.62
3	0.02129	60.72	1.09	3	0.01905	65.59	0.82
4	0.02559	56.25	1.39	4	0.02108	60.68	0.73
5	0.02711	55.97	1.09	5	0.02563	59.86	1.64
6	0.02875	56.28	0.67	6	0.02706	57.88	0.73
7	0.03091	57.34	0.94	7	0.02876	57.14	0.50
8	0.03325	53.78	1.09	8	0.03092	55.10	0.73
9	0.03941	51.23	0.41	9	0.03303	54.03	0.82
10	0.05096	45.32	1.19	10	0.04896	47.12	1.64
11	0.05223	40.32	1.34	11	0.05122	45.10	0.73
12	0.05450	43.03	0.77	12	0.05286	43.55	0.95
13	0.05715	39.61	1.34	13	0.05465	42.21	0.58
14	0.05836	42.73	1.89	14	0.05726	41.74	0.95
15	0.06089	36.78	1.34	15	0.05905	39.59	1.16
16	0.07306	35.14	1.09	16	0.06102	38.34	0.95
17	0.07518	34.80	1.09	17	0.07292	33.19	0.82
18	0.07705	34.24	1.09	18	0.07519	34.61	0.67
19	0.08136	31.86	1.09	19	0.07714	33.35	0.95
20	0.08510	31.15	1.34	20	0.07878	32.98	0.55
21	0.08748	29.09	0.39	21	0.08160	32.44	0.82
22	0.10073	25.45	1.09	22	0.08512	30.54	0.95
23	0.10310	23.95	0.94	23	0.08532	28.36	1.64
24	0.10403	24.22	1.89	24	0.08739	28.66	0.41
25	0.10683	23.62	0.67	25	0.08809	29.05	0.62
26	0.10965	25.06	1.89	26	0.09961	26.01	1.64
27	0.11067	23.30	1.34	27	0.10087	24.01	0.95
28	0.11230	23.30	1.89	28	0.10316	24.58	0.67
29	0.11521	21.35	0.94	29	0.10418	23.76	1.64
				30	0.10705	23.74	0.50
				31	0.10980	22.91	1.64
				32	0.11086	22.37	0.95
				33	0.11246	20.33	1.64
				34	0.11531	21.81	0.82
				35	0.11612	20.10	1.64



p=63.22 GeV/c

p=63.53 GeV/c

B=11.95 +/- 0.8 (C/GeV)\*\*2

B=11.50 +/- 0.11 (C/GeV)\*\*2

N	-t	$\frac{dG}{dt}$	$\Delta(\frac{dG}{dt})$	N	-t	$\frac{dG}{dt}$	$\Delta(\frac{dG}{dt})$
1	0.01378	71.36	0.47	1	0.01294	67.48	0.83
2	0.01297	69.51	0.70	2	0.01719	65.70	0.55
3	0.01977	62.77	0.70	3	0.01900	64.86	1.02
4	0.02381	63.24	0.63	4	0.02095	61.94	0.83
5	0.02564	58.32	0.99	5	0.02572	55.64	1.45
6	0.02728	59.27	0.63	6	0.02879	56.11	0.55
7	0.02876	56.60	0.42	7	0.03112	53.06	0.83
8	0.03113	55.57	0.63	8	0.03280	53.86	1.02
9	0.03306	53.14	0.53	9	0.04914	46.73	1.45
10	0.03953	50.81	0.27	10	0.05161	41.58	1.02
11	0.04906	46.29	1.40	11	0.05241	39.49	1.45
12	0.05111	44.41	1.31	12	0.05466	41.00	0.65
13	0.05233	43.52	0.99	13	0.05742	39.11	1.45
14	0.05456	43.41	0.53	14	0.05926	33.86	1.02
15	0.05736	39.75	1.40	15	0.06095	36.80	1.02
16	0.05896	41.52	0.81	16	0.07296	34.98	0.83
17	0.07309	35.04	0.70	17	0.07528	33.87	0.83
18	0.07519	33.34	0.70	18	0.07736	32.04	0.83
19	0.07711	34.24	0.63	19	0.07891	30.40	0.65
20	0.07877	32.16	0.53	20	0.08093	32.24	1.45
21	0.08075	32.24	1.40	21	0.08289	30.08	1.02
22	0.08301	30.13	0.81	22	0.08542	29.57	0.83
23	0.08532	30.07	0.63	23	0.08769	26.99	0.51
24	0.08758	28.97	0.31	24	0.08839	27.42	0.55
25	0.08930	27.88	1.40	25	0.09997	23.76	1.45
26	0.10037	24.83	0.63	26	0.10105	24.19	1.02
27	0.10339	23.53	0.70	27	0.10337	23.28	0.83
28	0.10421	23.97	0.81	28	0.10432	23.01	1.45
29	0.10705	23.15	0.39	29	0.10724	21.99	0.55
30	0.11070	22.79	0.81	30	0.11068	22.56	1.02
31	0.11267	23.89	0.99	31	0.11285	19.59	1.45
32	0.11514	20.75	0.63	32	0.11514	20.95	1.02
33	0.11625	19.31	1.40	33	0.11637	20.13	1.45

P=66.09GEV/C

P=69.18GEV/C

B=11.24+/-0.11(C/GEV)\*\*2

B=11.40+/-0.09(C/GEV)\*\*2

$N$	$-t$	$\frac{d\sigma}{dt}$	$\Delta\left(\frac{d\sigma}{dt}\right)$	$N$	$-t$	$\frac{d\sigma}{dt}$	$\Delta\left(\frac{d\sigma}{dt}\right)$
1	0.01064	70.55	0.55	1	0.01059	69.87	0.74
2	0.02111	61.53	0.72	2	0.01517	66.44	0.40
3	0.02575	55.81	1.44	3	0.01710	64.82	0.47
4	0.02695	59.31	0.72	4	0.01897	62.64	0.60
5	0.02897	55.85	0.51	5	0.02734	57.92	0.74
6	0.03109	54.23	0.72	6	0.02900	56.19	0.43
7	0.03335	54.40	1.02	7	0.03086	53.48	0.60
8	0.05133	42.91	1.02	8	0.03343	49.67	1.05
9	0.05218	44.91	0.83	9	0.03979	48.06	0.40
10	0.05491	41.12	0.59	10	0.05211	43.35	1.05
11	0.05750	39.57	1.02	11	0.05511	40.87	0.74
12	0.05971	38.70	1.44	12	0.05758	37.89	1.05
13	0.07371	31.42	1.44	13	0.06142	35.29	1.05
14	0.07535	33.51	0.72	14	0.07296	34.54	0.74
15	0.07628	32.84	1.44	15	0.07548	32.33	0.60
16	0.07890	31.90	0.51	16	0.08111	30.96	0.74
17	0.08101	30.10	1.44	17	0.08238	29.89	1.05
18	0.08275	30.45	0.83	18	0.08525	28.66	0.74
19	0.08514	29.13	1.44	19	0.08891	28.07	1.05
20	0.08769	28.38	0.51	20	0.08859	27.58	0.28
21	0.08848	26.98	0.54	21	0.10098	23.32	0.74
22	0.10114	23.93	1.02	22	0.10371	22.66	0.52
23	0.10344	23.93	0.64	23	0.10717	22.23	0.47
24	0.10442	23.50	1.44	24	0.10820	21.97	1.05
25	0.10737	22.06	0.59	25	0.11077	21.90	0.60
26	0.10806	23.16	1.02	26	0.11667	20.17	1.05
27	0.11099	21.66	0.83				
28	0.11296	21.56	1.44				
29	0.11567	20.23	1.44				
30	0.11653	19.22	1.02				

•• P= 9.43GEV/C

P=19.23GEV/C

$\alpha = -0.351 \pm 0.048$

$\alpha = -0.243 \pm 0.028$

N	-t	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$	N	-t	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$
1	0.00079	611.34	14.49	1	0.00106	365.07	4.36
2	0.00095	491.50	12.67	2	0.00125	302.48	5.53
3	0.00112	390.00	6.30	3	0.00146	244.08	4.70
4	0.00130	304.58	7.21	4	0.00168	209.18	2.68
5	0.00150	272.56	3.89	5	0.00191	192.49	4.55
6	0.00171	230.66	6.67	6	0.00192	185.92	2.77
7	0.00172	245.54	5.85	7	0.00217	159.26	3.22
8	0.00194	205.38	3.58	8	0.00244	142.13	3.01
9	0.00218	188.17	4.27	9	0.00272	145.23	2.13
10	0.00244	164.52	2.98	10	0.00302	127.57	2.84
11	0.00271	160.36	4.41	11	0.00334	121.77	1.96
12	0.00299	149.16	2.72	12	0.00366	114.03	1.72
13	0.00329	145.02	3.81	13	0.00367	120.17	2.26
14	0.00360	135.40	3.37	14	0.00401	106.10	3.31
15	0.00361	136.46	2.81	15	0.00402	110.77	1.88
16	0.00393	128.64	3.14	16	0.00437	108.16	5.19
17	0.00426	128.67	3.42	17	0.00475	103.23	2.31
18	0.00462	117.64	3.34	18	0.00514	101.42	2.11
19	0.00499	114.14	2.81	19	0.00555	98.58	2.09
20	0.00537	113.97	2.54	20	0.00597	93.79	1.34
21	0.00576	109.31	1.69	21	0.00642	93.34	0.99
22	0.00618	105.82	2.42	22	0.00687	94.82	2.65
23	0.00660	107.52	2.32	23	0.00734	89.10	3.82
24	0.00704	105.54	2.60	24	0.00782	86.82	1.85
25	0.00749	104.55	2.67	25	0.00833	87.55	1.73
26	0.00796	100.65	2.26	26	0.00885	84.14	1.71
27	0.00846	99.64	2.10	27	0.00940	86.86	1.15
28	0.00895	97.45	1.41	28	0.00994	82.92	0.84
29	0.00947	95.99	2.00	29	0.01052	82.53	2.23
30	0.00999	96.24	1.94	30	0.01110	78.41	3.49
31	0.01052	94.15	2.20	31	0.01169	78.93	1.64
32	0.01108	91.37	2.20	32	0.01231	78.08	1.51
33	0.01165	90.53	1.92	33	0.01294	79.83	1.52
34	0.01283	88.66	1.61	34	0.01359	77.80	1.29
				35	0.01426	77.15	1.11

P=30.42GEV/C

P=55.38GEV/C

$\alpha = -0.176 \pm 0.022$

$\alpha = -0.154 \pm 0.023$

N	-t	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$	N	-t	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$
1	0.00107	332.80	6.81	1	0.00079	513.97	21.49
2	0.00124	268.41	5.07	2	0.00096	391.69	6.34
3	0.00132	267.10	6.49	3	0.00115	304.04	4.71
4	0.00143	224.65	4.62	4	0.00136	239.57	8.19
5	0.00152	226.95	3.83	5	0.00158	198.88	4.25
6	0.00162	202.63	3.84	6	0.00181	174.50	4.67
7	0.00172	193.28	4.49	7	0.00182	173.44	2.83
8	0.00181	182.97	5.02	8	0.00207	151.00	2.63
9	0.00195	162.78	3.91	9	0.00234	141.76	3.01
10	0.00203	168.85	3.67	10	0.00263	125.61	2.81
11	0.00218	156.67	3.12	11	0.00293	118.05	2.00
12	0.00229	145.15	3.53	12	0.00325	107.30	2.60
13	0.00242	138.55	2.91	13	0.00359	104.21	1.84
14	0.00254	131.41	2.25	14	0.00394	101.96	2.14
15	0.00268	127.31	2.37	15	0.00395	98.71	2.10
16	0.00281	124.36	2.76	16	0.00432	97.23	1.53
17	0.00310	118.90	2.48	17	0.00470	98.95	4.78
18	0.00338	107.81	2.09	18	0.00510	89.05	2.12
19	0.00357	106.03	2.48	19	0.00553	86.64	1.94
20	0.00369	104.41	1.94	20	0.00597	83.50	1.91
21	0.00388	101.89	2.13	21	0.00642	84.97	1.26
22	0.00400	97.82	1.57	22	0.00684	91.33	1.64
23	0.00423	101.66	2.16	23	0.00690	79.23	1.40
24	0.00457	94.52	1.49	24	0.00737	90.48	2.40
25	0.00493	92.48	1.91	25	0.00788	75.46	3.56
26	0.00531	90.03	1.81	26	0.00839	78.66	1.73
27	0.00568	88.56	1.52	27	0.00893	77.21	1.61
28	0.00607	90.26	1.54	28	0.00949	76.22	1.64
29	0.00636	87.38	1.77	29	0.01007	74.84	1.06
30	0.00647	84.83	1.27	30	0.01067	74.17	0.61
31	0.00678	83.79	1.60	31	0.01128	73.00	2.07
32	0.00724	80.84	1.65	32	0.01190	75.97	3.20
33	0.00768	82.78	1.17	33	0.01253	70.72	1.52
34	0.00814	81.35	1.54	34	0.01319	71.16	1.38
35	0.00863	80.36	1.47	35	0.01387	67.98	1.41
36	0.00910	81.71	1.28	36	0.01456	70.28	1.20
37	0.00960	76.79	1.24	37	0.01527	68.03	1.07
38	0.00999	75.63	1.56				
39	0.01010	79.18	1.06				
40	0.01051	73.89	1.40				
41	0.01108	73.97	1.49				
42	0.01163	73.36	1.05				
43	0.01220	72.42	1.35				
44	0.01279	74.08	1.31				
45	0.01336	71.55	1.14				
46	0.01396	72.35	1.13				
47	0.01457	71.45	0.92				

•• E=59.40GEV/c

P=69.84GEV/c

$\Delta = -0.122 \pm 0.020$

$\Delta = -0.106 \pm 0.020$

N	-t	$\frac{dG}{dt}$	$\Delta(\frac{dG}{dt})$	N	-t	$\frac{dG}{dt}$	$\Delta(\frac{dG}{dt})$
1	0.00079	501.78	13.39	1	0.00110	306.77	6.70
2	0.00096	380.55	8.41	2	0.00127	248.46	4.93
3	0.00115	295.37	4.70	3	0.00136	245.15	6.79
4	0.00136	244.27	4.03	4	0.00146	201.55	4.33
5	0.00155	202.47	5.38	5	0.00155	201.67	3.88
6	0.00157	211.10	6.73	6	0.00166	174.08	3.53
7	0.00158	199.79	6.92	7	0.00177	171.77	4.42
8	0.00181	164.72	5.19	8	0.00185	175.21	4.99
9	0.00182	165.51	3.08	9	0.00200	152.85	3.87
10	0.00207	145.87	2.63	10	0.00208	155.00	3.92
11	0.00234	135.39	2.32	11	0.00223	131.44	3.02
12	0.00259	120.67	3.26	12	0.00235	134.59	3.61
13	0.00263	124.22	2.41	13	0.00248	126.45	2.90
14	0.00293	114.93	1.72	14	0.00260	120.95	2.19
15	0.00325	105.56	1.93	15	0.00274	116.72	2.37
16	0.00359	99.56	1.71	16	0.00288	114.26	2.73
17	0.00391	98.30	2.22	17	0.00317	106.27	2.43
18	0.00395	98.68	2.17	18	0.00346	97.32	2.02
19	0.00432	99.10	1.34	19	0.00365	101.15	2.40
20	0.00470	93.10	2.69	20	0.00377	97.29	1.92
21	0.00511	86.59	1.45	21	0.00397	94.33	2.17
22	0.00553	86.61	1.29	22	0.00409	91.48	1.54
23	0.00597	81.29	1.43	23	0.00433	88.73	2.14
24	0.00637	80.86	1.74	24	0.00468	98.69	1.53
25	0.00642	82.34	1.74	25	0.00504	88.13	1.91
26	0.00690	77.36	1.10	26	0.00543	84.00	1.79
27	0.00738	79.36	1.43	27	0.00580	84.27	1.52
28	0.00788	74.16	2.06	28	0.00621	81.31	1.50
29	0.00840	75.53	1.78	29	0.00650	77.54	1.69
30	0.00843	73.91	1.66	30	0.00662	80.96	1.29
31	0.00894	75.82	1.42	31	0.00693	77.71	1.56
32	0.00897	76.96	1.65	32	0.00740	78.51	1.64
33	0.00950	73.49	1.47	33	0.00788	74.87	1.16
34	0.00952	76.67	2.05	34	0.00833	74.26	1.49
35	0.01001	73.27	1.43	35	0.00882	75.46	1.44
36	0.01010	70.17	1.51	36	0.00930	74.26	1.26
37	0.01067	72.55	0.96	37	0.00981	73.80	1.25
38	0.01129	71.69	1.27	38	0.01021	71.28	1.52
39	0.01191	71.39	1.90	39	0.01032	75.07	1.07
40	0.01255	71.05	1.54	40	0.01074	69.78	1.39
41	0.01321	69.59	1.25	41	0.01133	67.73	1.50
42	0.01388	70.36	1.36	42	0.01189	70.40	1.05
43	0.01450	67.54	1.29	43	0.01247	68.00	1.36
44	0.01529	69.28	1.14	44	0.01307	57.45	1.31
				45	0.01366	69.96	1.13
				46	0.01427	67.70	1.12
				47	0.01489	65.80	0.93

\*\*  $E=69.34\text{GeV}/c$

$$\alpha = -0.083 \pm 0.016$$

$N$	$-t$	$\frac{d\sigma}{dt}$	$\Delta\left(\frac{d\sigma}{dt}\right)$	$N$	$-t$	$\frac{d\sigma}{dt}$	$\Delta\left(\frac{d\sigma}{dt}\right)$
1	0.00105	522.17	7.23	19	0.00667	78.34	1.12
2	0.00125	252.65	5.95	20	0.00715	76.58	1.48
3	0.00146	207.91	3.21	21	0.00765	76.54	1.47
4	0.00169	173.52	2.32	22	0.00870	73.64	1.04
5	0.00193	155.03	3.38	23	0.00925	72.05	1.04
6	0.00194	15.98	2.63	24	0.00982	73.70	0.99
7	0.00220	134.43	2.20	25	0.01040	71.69	0.97
8	0.00248	120.66	1.89	26	0.01101	69.28	0.97
9	0.00278	114.17	1.51	27	0.01163	67.78	1.29
10	0.00309	105.15	1.41	28	0.01291	65.31	0.90
11	0.00342	98.86	1.57	29	0.01358	67.08	0.89
12	0.00377	92.49	1.38	30	0.01426	67.20	0.86
13	0.00413	92.23	1.43	31	0.01497	65.58	0.84
14	0.00451	85.80	1.84	32	0.01568	65.00	0.84
15	0.00452	88.04	1.97	33	0.01641	63.11	1.33
16	0.00532	82.54	1.24	34	0.01792	63.19	1.32
17	0.00575	81.74	1.21	35	0.01952	61.84	0.98
18	0.00620	75.56	1.14	36	0.02035	62.22	1.07

\*\*\*

P=18.90GEV/C

$\alpha = -0.259 \pm 0.027$

B=10.24  $\pm$  0.11

N	-t	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$	N	-t	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$
1	0.00090	469.18	9.22	35	0.01112	82.16	1.73
2	0.00107	371.35	7.36	36	0.01172	81.62	1.53
3	0.00126	294.99	3.89	37	0.01233	80.01	1.29
4	0.00145	245.19	5.52	38	0.01354	79.04	1.29
5	0.00147	247.43	6.89	39	0.01428	77.05	1.19
6	0.00169	219.50	3.50	40	0.01474	77.61	0.69
7	0.00193	171.44	2.67	41	0.01677	75.07	0.61
8	0.00218	164.51	2.22	42	0.02002	73.52	1.38
9	0.00242	162.45	3.51	43	0.02691	65.43	0.79
10	0.00245	158.50	2.43	44	0.02918	65.95	0.97
11	0.00274	139.49	1.72	45	0.03115	63.31	0.97
12	0.00304	13.83	2.93	46	0.03687	58.77	0.57
13	0.00335	123.32	1.72	47	0.04716	53.36	1.38
14	0.00365	115.39	2.25	48	0.04918	53.63	1.38
15	0.00363	115.56	2.18	49	0.05123	49.78	0.97
16	0.00403	112.97	1.79	50	0.05375	48.82	1.38
17	0.00404	104.73	2.05	51	0.05447	50.65	1.38
18	0.00439	113.20	2.55	52	0.05719	46.46	1.38
19	0.00477	101.20	1.43	53	0.06875	40.89	0.97
20	0.00515	101.57	1.30	54	0.07115	42.86	0.97
21	0.00557	98.84	1.50	55	0.07341	39.56	0.79
22	0.00595	95.61	1.75	56	0.07411	39.57	1.38
23	0.00600	95.52	1.70	57	0.07731	39.14	0.97
24	0.00643	92.33	1.14	58	0.07989	38.64	1.38
25	0.00633	93.33	1.38	59	0.08155	36.61	0.49
26	0.00736	88.43	1.98	60	0.08224	35.52	0.52
27	0.00784	91.90	1.75	61	0.09509	31.03	1.38
28	0.00836	87.32	1.09	62	0.09742	30.37	0.97
29	0.00888	97.83	1.25	63	0.09977	29.44	0.97
30	0.00902	85.45	3.56	64	0.10071	29.06	0.97
31	0.00935	84.58	1.47	65	0.10454	29.60	0.93
32	0.00943	86.21	1.51	66	0.10744	29.15	1.38
33	0.00997	83.24	1.98	67	0.10883	26.91	1.38
34	0.01054	82.56	1.21				

... P=33.315EV/c  
 $\alpha = -0.171 + i - 0.029$   
 $B = 10.687 - 0.09$

N	-t	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$	N	-t	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$
1	0.00086	463.39	13.05	34	0.01254	70.33	2.22
2	0.00103	360.36	12.19	35	0.01331	72.49	1.75
3	0.00123	282.74	5.75	36	0.01397	71.67	1.67
4	0.00143	234.32	7.00	37	0.01467	72.47	1.88
5	0.00144	227.86	4.88	38	0.01709	59.59	0.42
6	0.00166	200.22	3.55	39	0.02100	57.22	0.73
7	0.00190	164.98	3.92	40	0.02713	50.92	0.65
8	0.00216	155.28	3.19	41	0.02837	59.67	1.52
9	0.00243	137.63	2.90	42	0.03390	59.40	1.51
10	0.00272	121.72	2.34	43	0.03242	51.54	0.92
11	0.00303	114.24	2.77	44	0.04894	47.63	0.92
12	0.00335	107.25	2.20	45	0.05111	45.24	0.63
13	0.00369	105.62	3.17	46	0.05365	46.72	0.52
14	0.00370	100.17	2.82	47	0.05402	40.15	1.27
15	0.00405	94.77	2.14	48	0.05573	43.73	0.73
16	0.00442	97.85	2.87	49	0.05892	43.29	1.27
17	0.00481	95.17	2.76	50	0.06008	41.29	0.90
18	0.00522	92.40	2.18	51	0.07130	35.02	1.27
19	0.00564	88.72	1.70	52	0.07274	37.94	0.73
20	0.00603	84.73	1.03	53	0.07471	35.70	0.73
21	0.00654	83.65	1.72	54	0.07753	34.18	0.45
22	0.00700	84.42	2.31	55	0.08298	32.67	0.92
23	0.00749	81.22	2.23	56	0.08463	32.84	0.73
24	0.00799	84.32	2.26	57	0.08625	31.42	0.34
25	0.00851	82.57	2.53	58	0.08970	32.88	0.92
26	0.00905	79.42	1.52	59	0.09962	26.56	0.92
27	0.00962	77.40	1.41	60	0.10132	26.35	0.92
28	0.01019	77.04	1.51	61	0.10255	25.41	0.92
29	0.01079	74.75	1.98	62	0.10557	25.69	0.45
30	0.01128	75.35	1.03	63	0.10922	24.79	0.92
31	0.01139	72.83	1.95	64	0.11078	25.00	1.27
32	0.01200	72.55	1.39	65	0.11318	24.41	0.92
33	0.01258	74.22	1.73				



$P = 40.52 \text{ E.V./C}$   
 $\alpha = -0.16g + / - 0.021$   
 $\beta = 10.82 + / - 0.11$

N	t	$\frac{d\sigma}{dt}$	$\Delta(\frac{d\sigma}{dt})$	N	t	$\frac{d\sigma}{dt}$	$\Delta(\frac{d\sigma}{dt})$
1	0.00038	434.15	0.76	34	0.01270	72.26	1.53
2	0.00106	344.42	0.49	35	0.01342	69.62	1.21
3	0.00125	274.66	3.49	36	0.01410	70.00	1.20
4	0.00146	221.15	2.84	37	0.01479	58.39	1.30
5	0.00159	181.24	2.39	38	0.01713	59.34	0.50
6	0.00193	167.41	4.32	39	0.02107	57.01	0.83
7	0.00194	163.52	3.48	40	0.02845	59.63	0.58
8	0.00225	149.04	2.20	41	0.03068	58.18	0.83
9	0.00247	132.82	2.10	42	0.03301	56.49	0.83
10	0.00275	122.83	2.44	43	0.03900	52.53	0.31
11	0.00377	111.44	2.18	44	0.04957	43.88	1.43
12	0.00383	111.16	1.91	45	0.05126	43.92	0.71
13	0.00393	104.22	1.55	46	0.05377	44.74	0.83
14	0.00373	104.59	1.49	47	0.05411	44.83	0.83
15	0.00411	93.24	1.40	48	0.05696	43.46	0.83
16	0.00443	91.40	2.14	49	0.05027	42.81	1.01
17	0.00437	94.61	1.83	50	0.07297	37.20	0.83
18	0.00528	81.80	1.44	51	0.07494	35.19	0.83
19	0.00573	35.50	1.26	52	0.07770	34.72	0.71
20	0.00615	82.55	1.15	53	0.07800	32.88	1.01
21	0.00661	33.57	1.23	54	0.08044	33.33	1.01
22	0.00708	31.33	1.62	55	0.08233	33.92	1.43
23	0.00757	31.25	1.66	56	0.08509	32.60	0.83
24	0.00807	31.43	1.48	57	0.08652	30.57	0.38
25	0.00850	75.33	1.75	58	0.09979	27.01	1.43
26	0.00915	77.31	1.06	59	0.10061	26.19	1.01
27	0.00971	77.69	1.00	60	0.10262	25.64	0.83
28	0.01029	77.14	1.06	61	0.10572	25.22	0.83
29	0.01089	72.80	1.40	62	0.10618	24.95	0.83
30	0.01119	74.53	0.83	63	0.10955	25.01	1.01
31	0.01149	75.27	1.48	64	0.11113	24.92	1.43
32	0.01211	72.59	1.24	65	0.11379	23.97	1.43
33	0.01262	71.73	0.83				

$\rho = 59.52 \text{ Ev/c}$   
 $\alpha = -0.139 + i - 11.030$   
 $\beta = 13.34 + i - 3.11$

$N$	$-t$	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$	$N$	$-t$	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$
1	0.00096	373.37	1.49	34	0.01381	71.39	1.54
2	0.00115	304.70	9.08	35	0.01517	70.65	0.77
3	0.00135	257.43	5.23	36	0.01521	59.44	1.37
4	0.00157	214.19	5.38	37	0.01927	67.14	0.95
5	0.00181	174.54	5.63	38	0.02121	63.29	0.95
6	0.00181	175.02	3.98	39	0.02727	59.87	0.35
7	0.00206	143.76	3.85	40	0.02864	57.53	0.57
8	0.00233	132.02	3.07	41	0.03082	57.09	0.95
9	0.00261	123.72	3.25	42	0.03291	55.79	0.95
10	0.00292	115.54	2.34	43	0.03925	52.00	0.35
11	0.00324	111.43	3.34	44	0.04931	44.61	1.34
12	0.00358	103.36	2.25	45	0.05109	44.28	0.95
13	0.00393	102.22	4.39	46	0.05262	43.40	1.29
14	0.00430	100.13	2.12	47	0.05429	44.14	0.57
15	0.00468	92.97	2.43	48	0.05693	44.43	1.09
16	0.00508	94.74	2.71	49	0.05870	42.02	1.34
17	0.00553	90.69	2.67	50	0.06063	41.10	1.09
18	0.00594	83.07	2.14	51	0.07183	32.80	1.39
19	0.00639	84.61	2.72	52	0.07311	33.63	1.09
20	0.00687	82.17	1.55	53	0.07524	34.25	0.95
21	0.00734	81.65	2.72	54	0.07779	31.40	1.89
22	0.00784	76.39	1.83	55	0.07833	35.09	0.67
23	0.00836	77.37	2.14	56	0.08146	33.73	1.09
24	0.00890	77.02	2.14	57	0.08291	35.83	1.39
25	0.00926	75.72	0.55	58	0.08531	31.29	0.95
26	0.00945	75.06	1.74	59	0.08707	29.71	0.41
27	0.01005	74.55	2.23	60	0.09911	25.89	1.34
28	0.01052	73.35	1.31	61	0.10091	24.45	0.95
29	0.01123	71.26	2.19	62	0.10337	24.05	0.95
30	0.01135	71.33	1.56	63	0.10656	23.66	0.53
31	0.01248	71.07	1.80	64	0.11066	24.07	0.95
32	0.01268	69.35	1.09	65	0.11374	22.29	1.89
33	0.01314	72.10	1.83	66	0.11503	22.13	0.95

...  $D=69.347 \text{ EV/C}$   
 $\alpha = -0.136 \pm 0.023$   
 $H = 11.48 \pm 0.15$

N	-t	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$	N	-t	$\frac{dG}{dt}$	$\Delta\left(\frac{dG}{dt}\right)$
1	0.00111	292.45	11.39	38	0.01517	65.58	1.33
2	0.00131	237.33	3.93	39	0.01525	67.38	0.81
3	0.00153	194.23	4.85	40	0.01590	64.27	1.22
4	0.00175	172.77	3.50	41	0.01663	63.27	1.65
5	0.00201	147.75	5.24	42	0.01734	64.85	1.51
6	0.00202	156.74	3.86	43	0.01752	66.48	0.94
7	0.00228	134.21	3.25	44	0.01815	65.26	1.64
8	0.00257	119.42	2.91	45	0.01895	63.93	1.69
9	0.00287	113.24	2.29	46	0.01907	64.91	1.15
10	0.00319	104.57	2.15	47	0.01976	61.93	1.58
11	0.00352	94.33	2.46	48	0.02059	61.42	1.71
12	0.00384	98.19	2.17	49	0.02144	62.33	1.67
13	0.00424	92.33	2.87	50	0.02157	58.85	1.63
14	0.00425	91.73	3.21	51	0.02581	56.45	1.63
15	0.00463	85.48	2.76	52	0.02737	57.15	1.63
16	0.00464	89.86	3.09	53	0.02906	54.79	0.83
17	0.00503	89.55	2.52	54	0.03091	53.64	1.15
18	0.00545	80.55	1.44	55	0.03549	49.28	1.92
19	0.00584	87.45	1.67	56	0.03982	47.84	0.65
20	0.00634	75.95	1.79	57	0.05143	44.18	1.63
21	0.00681	75.40	1.69	58	0.05515	40.15	1.15
22	0.00730	73.54	1.64	59	0.05762	39.14	1.63
23	0.00780	70.91	2.22	60	0.06140	35.41	1.63
24	0.00832	72.95	1.46	61	0.07304	33.94	1.63
25	0.00846	75.49	1.63	62	0.07533	33.11	1.15
26	0.00836	75.25	1.65	63	0.07885	30.60	0.83
27	0.00942	71.59	1.59	64	0.08121	34.13	1.63
28	0.00999	73.14	1.54	65	0.08244	28.88	1.63
29	0.01040	58.77	3.94	66	0.08535	30.44	1.63
30	0.01058	71.17	1.49	67	0.08697	28.48	1.63
31	0.01119	69.77	1.45	68	0.08869	27.33	0.63
32	0.01182	77.73	1.97	69	0.10119	23.57	1.53
33	0.01245	64.14	1.76	70	0.10335	24.72	1.63
34	0.01310	67.33	1.92	71	0.10407	22.62	1.63
35	0.01318	64.17	1.63	72	0.10709	21.32	1.15
36	0.01378	65.35	1.37	73	0.10817	21.28	1.15
37	0.01447	64.54	1.33				